



Baltic  
InteGrid

Integrated Baltic Offshore  
Wind Electricity Grid Development

# Technology options and development trends for OWE and grids

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DTU Wind Energy

**Wind**  
EUROPE CONFERENCE  
& EXHIBITION  
2017 28-30 NOVEMBER  
AMSTERDAM

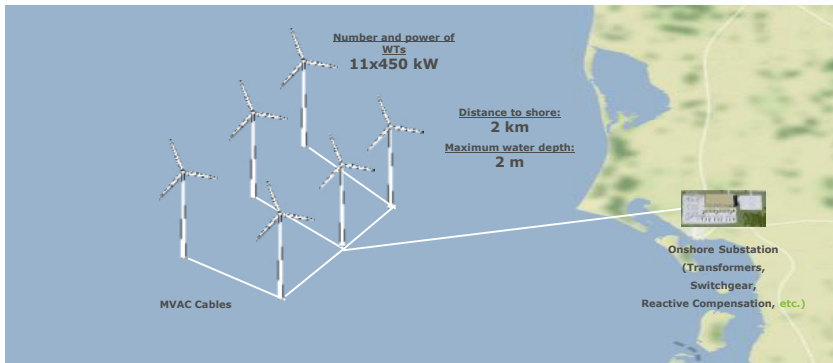
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**Interreg**  
Baltic Sea Region



EUROPEAN  
REGIONAL  
DEVELOPMENT  
FUND

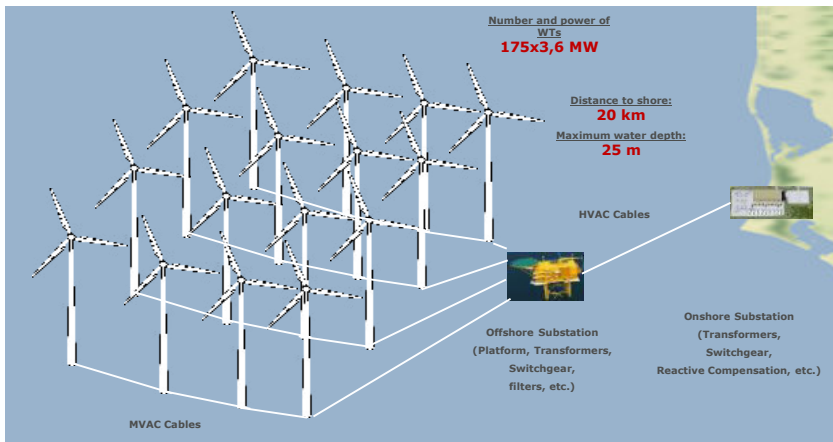


Wind Farm: Vindeby in Denmark. First installed Wind Farm in the world back in the year 1991.

Source: <https://wattsupwiththat.com/2017/03/22/by-the-numbers-lifetime-performance-of-worlds-first-offshore-wind-farm/>



**LCOE: 16 cents of €/kWh (2017 Euro)**



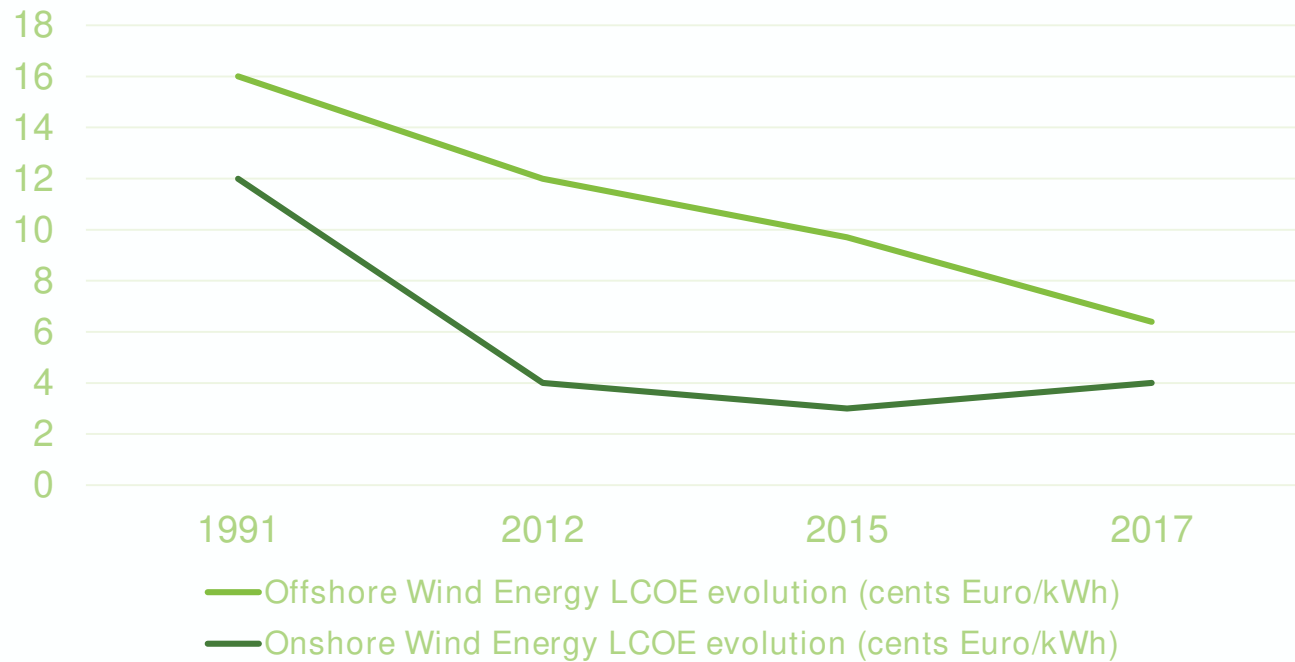
Wind Farm: London array in UK. Largest installed Wind Farm under operation in the world currently.

Source: <https://renewablesnow.com/news/study-says-gbp-100mwh-lcoe-for-uk-offshore-wind-achievable-by-2020-465585/>



**LCOE: 12 cents of €/kWh (2017 Euro)**

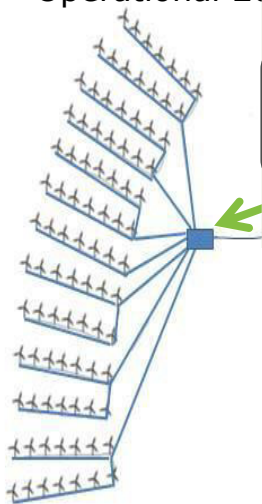
## LCOE Evolution of Wind Energy Projects



### Horns Rev 2

91 WT x 2.3  
MW=209 MW

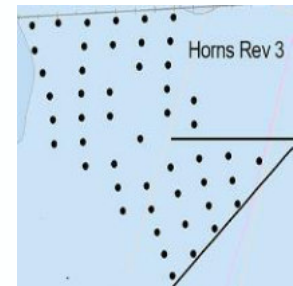
Operational 2000



### Horns Rev 3

49 WT x 8.3  
MW=406.7 MW

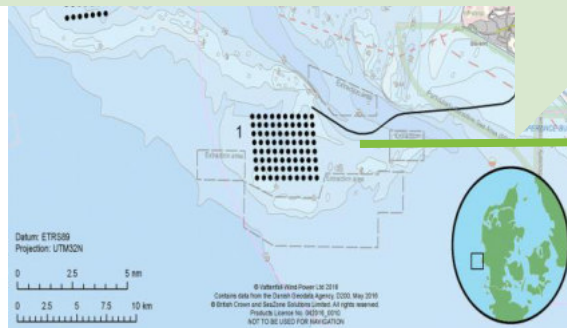
Operational 2020



Grid-based  
micrositing  
design

Polar-based  
micrositing  
design

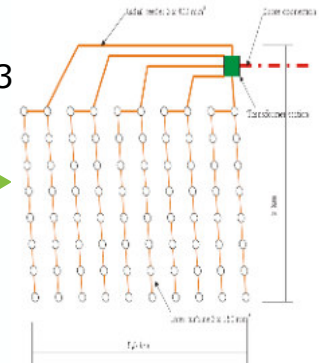
Coordinate-  
based  
micrositing  
design



### Horns Rev 1

160 WT x 2.0  
MW=160 MW

Operational 2003



$$LCOE = \frac{CAPEX + OPEX}{AEP}$$

LCOE: Levelized Cost of Energy

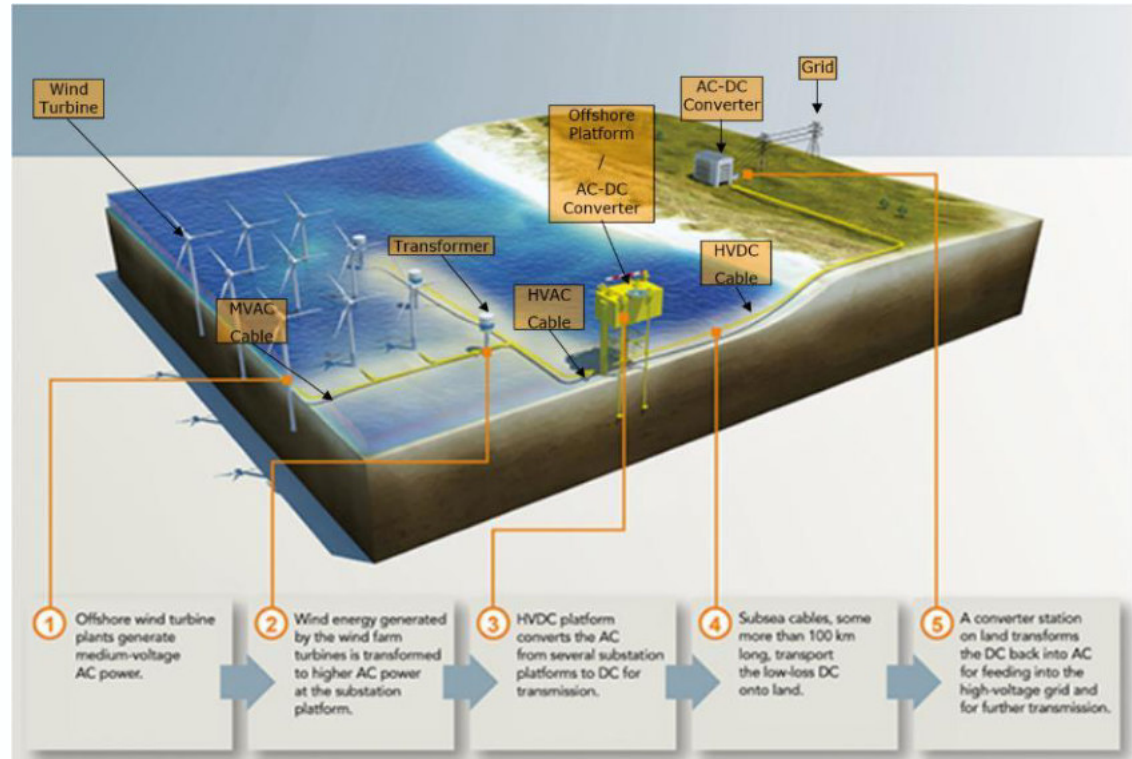
CAPEX: Capital investment expenditures

OPEX: Operation and maintenance cost

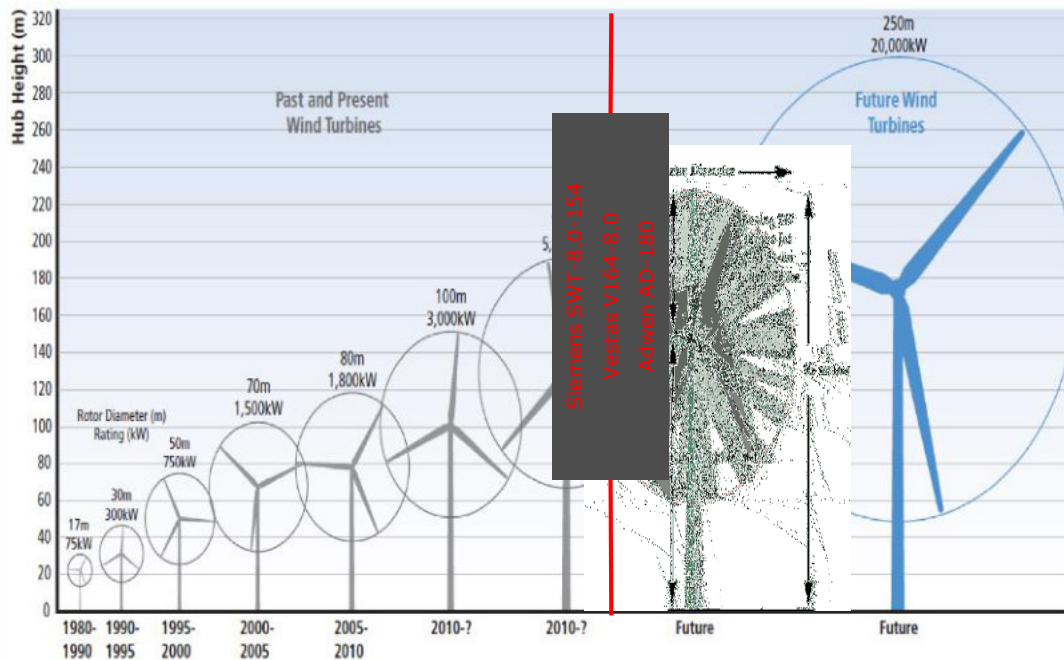
AEP: Annual Energy Production

### Minimizing LCOE

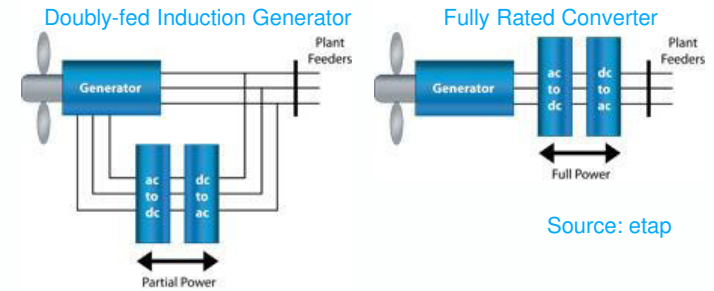
- **Minimizing CAPEX**
- **Minimizing OPEX**
- **Maximizing AEP**



Source: tdworld.com

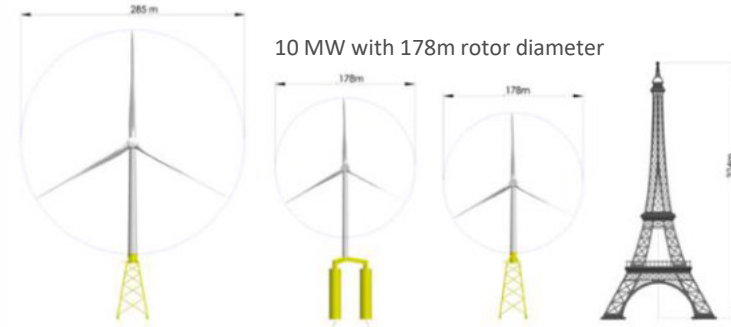


Source: Wiser et al. (2011). Wind Energy. In IPCC Special Report on Renewable Energy Sources and Climate Change Mitigation. Cambridge: Cambridge University Press.



Source: etap

20 MW with 285m rotor diameter



Source: INNWIND.EU

### Cross-linked polyethylene (XLPE) cable

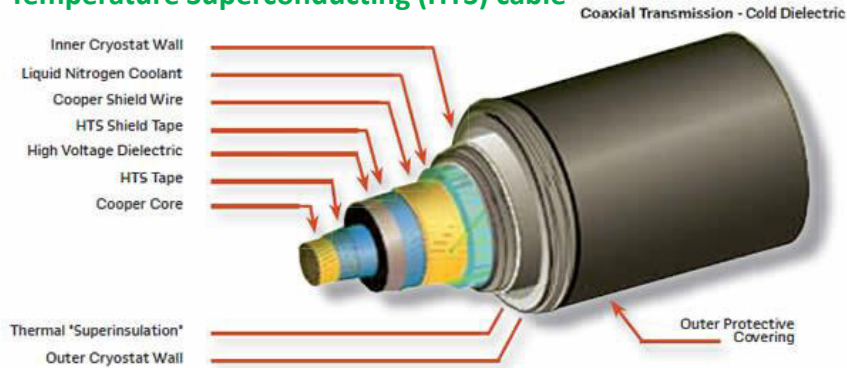


Source: Electrical India

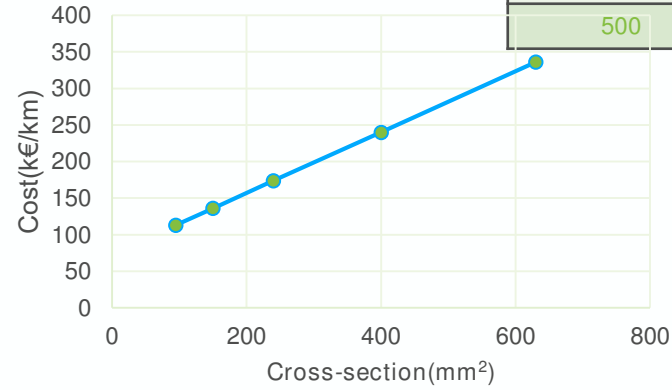
- Length: 20-100 km depending on voltage rating and shunt compensation
- Maximum Voltage: 500 kV
- Current Rating: 1.9-2.6 kA

Rated Voltage (kV)	Cross-section (mm <sup>2</sup> )
66	240-2000
110	400-2500
132	400-2500
150	400-2500
220	630-2500
275	630-2500
345	800-2500
400	800-2500
500	1600-2500

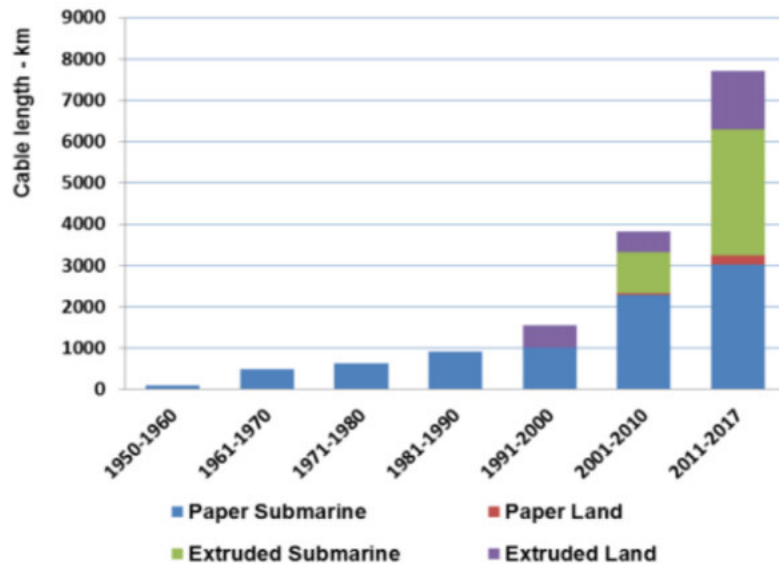
### High Temperature Superconducting (HTS) cable



Source: PAC World



- Self-Contained Fluid Filled Cables
- Mass Impregnated Cables
- Cross-Linked Poly-Ethylene Cables



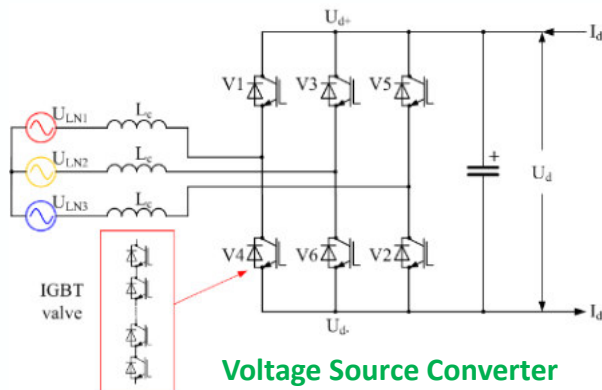
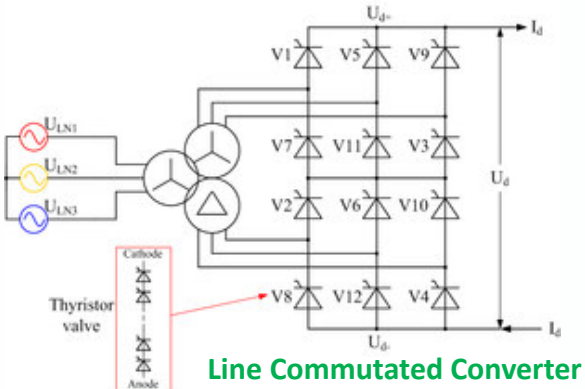
### Typical Data

- Transmission Distance: >1000 km
- Typical losses per circuit (bipole): 27 W/m (21 W/m in future)
- Maximum Voltage: 400-525-640 kV
- Current rating: 1900 kA
- Max Power per VSC substation (bipole): 1524-1710MW(1710-1895MW in future)
- Max Power per LCC substation (bipole): 600 MW
- Cross-section Area: 3000 mm<sup>2</sup> for 2000 MW at 250 kV in Kii Channel
- Deep sea installations: 500 m (1000 m in future)

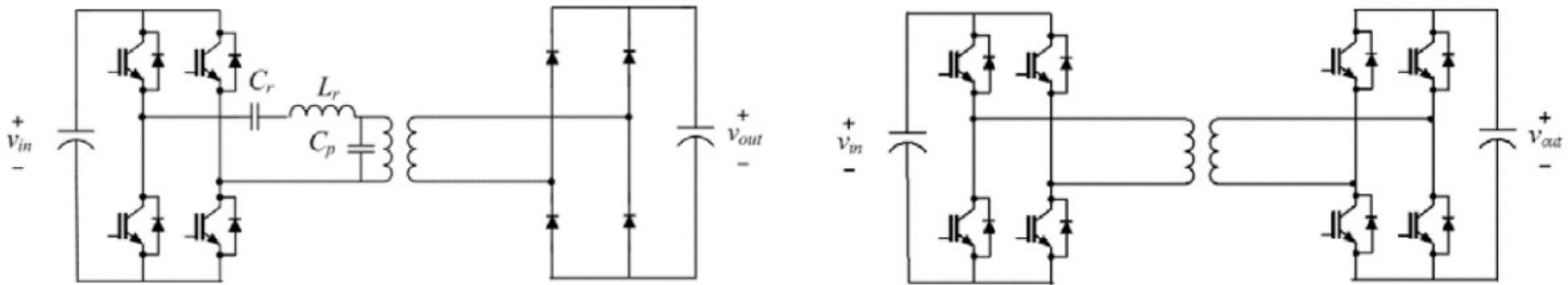
### Cost Example: XLPE HVDC cables

- Capex: 1470-1625 k€/ km (Installation costs: 29%)
- Opex: 2.9-3.2 k€/km
- Lifespan: >40 years

Source: E. Zaccone, High voltage underground and subsea cable technology options for future transmission in Europe, presentation at E-Highway2050 WP3 workshop, 2014

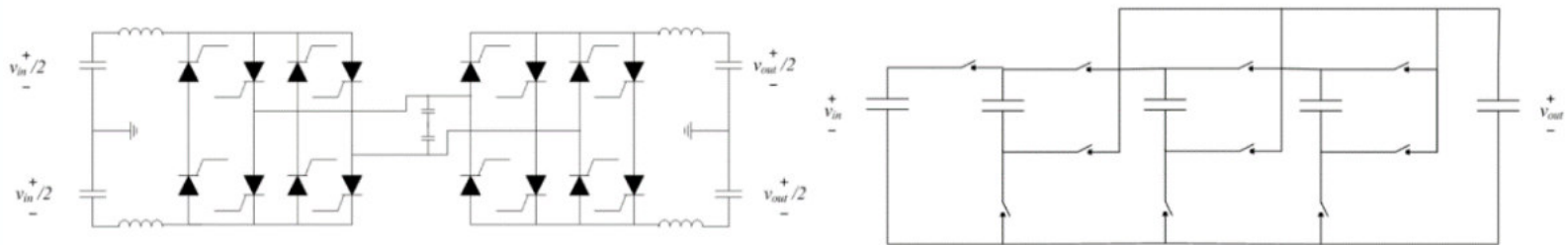


Line Commutated Converters	Voltage Source Converters
<ul style="list-style-type: none"> <li>• Since early 1950</li> <li>• Typically uses thyristors</li> <li>• More powerful, lower losses</li> <li>• Requires more space</li> <li>• Induces more severe requirements for cables</li> </ul>	<ul style="list-style-type: none"> <li>• Since 1999</li> <li>• Uses IGBTs, GTOs, etc.</li> <li>• Currently limited in power &amp; voltage</li> <li>• More controllable, flexible, smaller and lighter</li> <li>• Allows independent control of active and reactive power</li> </ul>
<p><u>Typical Data</u></p> <ul style="list-style-type: none"> <li>• Voltage (line to ground) for converter: 800-1100 kV</li> <li>• Voltage (line to ground) for cables: 550 kV</li> <li>• Current: 4-5 kA (6 kA in future)</li> <li>• Max Power per substation (bipole) : 8-11 GW (upto 13.2 GW in future)</li> <li>• Maximum length of the line: 2000 km</li> <li>• Maximum length of the cable: 580-600 km</li> <li>• Transmission Losses: 0.7-1.1% of rated power per converter station</li> </ul>	<p><u>Typical Data</u></p> <ul style="list-style-type: none"> <li>• Voltage (line to ground) for converter: 500-800 kV</li> <li>• Voltage (line to ground) for cables: 500 kV</li> <li>• Current: 1.5-3 kA (3-4 kA in future)</li> <li>• Max Power per substation (bipole) : 2000-4800 MW (6400 MW in future)</li> <li>• Maximum length of the line: 700-2000 km (3000 km in future)</li> <li>• Maximum length of the cable: 400 km (600-1000 km in future)</li> <li>• Transmission Losses: 0.9-1.3% of rated power (0.7-1.1% in future) per converter station.</li> </ul>



Isolated DC-DC converters

left: Resonant bridge converter; right: Dual active bridge converter



Non-isolated DC-DC converters

left: Bidirectional high-power DC transformer; right: Modular multi-level capacitor clamped DC-DC converter

## 2 ways to mitigate harmonics in WPPs –

- Avoiding harmonic resonance and emission by appropriate design
- Use of harmonic filters

### Passive Filter

- A bank of tuned LC filters and/or low-pass/high-pass filter
- Low initial cost and high efficiency
- Disadvantages-
  - Strongly depended on source impedance
  - Excessive harmonic currents can flow due to resonance

### Technical feasibilities

Voltage : 550 kV

Power : >3 Mvar

### Active Filter

- They consist of voltage- or current-source PWM inverters and have the ability to overcome the inherent disadvantages in passive filters
- Hybrid filter consists of mainly two parts-
  - Passive part comprises of a double tuned passive filter
  - Active part consists of - Current transducer, Control system, Amplifier, Transformer, Protection Circuit and arrester, Bypass switch and disconnectors

### Technical feasibilities

Voltage : 500 kV

Filtering frequency range :

350-2500 Hz (Chandrapur-Padghe HVDC)

300-3000 Hz (Baltic Cable HVDC Link)

## Reactive Compensation

### Shunt Compensation

### Series Compensation

#### Static Var Compensator (SVC)

Voltage : 765 kV  
 Dynamic Q : -300/+600 MVar  
 Current : 4-5 kA per branch

Capex : 30-50 k€/MVAR  
 (Average investment cost ranges for a SVC at 2013, rating: 100-850 MVAR/MVA; 400 kV)

#### Static Synchronous Compensator (STATCOM)

Voltage : 765 kV  
 Dynamic Q : -200/+200MVar  
 Current : 2-3 kA per branch

Capex : 50-75 k€/MVAR  
 (Average investment cost ranges for a STATCOM at 2013, rating: 100-400 MVAR/MVA; 400 kV)

#### Fixed Series Capacitor

Voltage : 765 kV  
 Rated Q : 1350 MVar

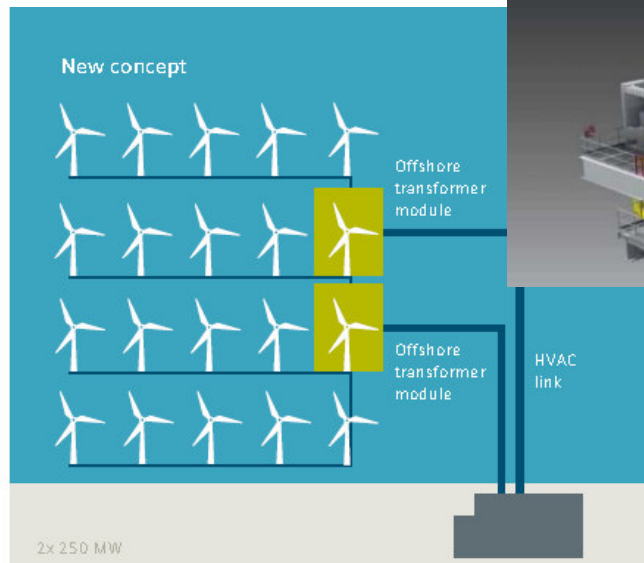
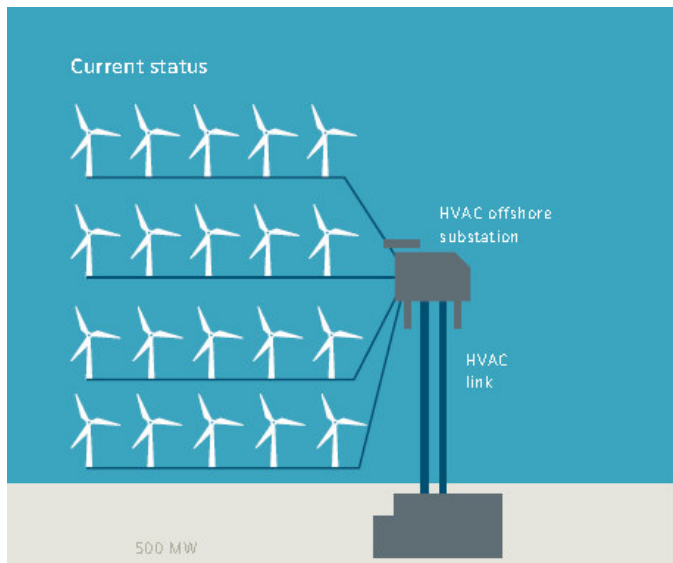
Capex : 10-20 k€/MVAR  
 (Average investment cost ranges for a FSC at 2013, rating: 100-1000 MVAR/MVA; 400 kV)

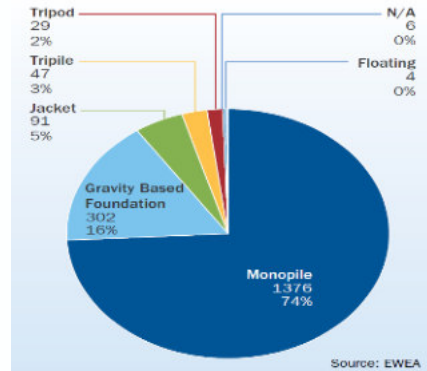
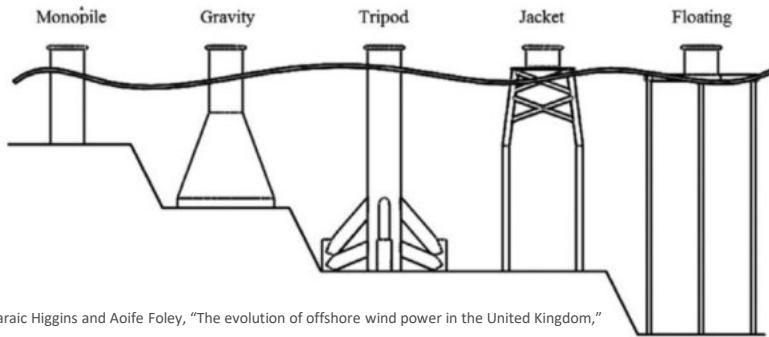
#### Thyristor Controlled Series Compensation (TCSC)

Voltage: 400-550 kV  
 Current: 1500 A  
 Power: 493 MVar

## Typical Data

- Voltage (line to ground): 765 kV
- Current: 10 kA (Not a limiting factor)
- Max Power per unit: dictated by cables (Typical 765 kV transformers have power rating close to 800 MVA)
- Losses per unit: 0.2-0.4% of rated power

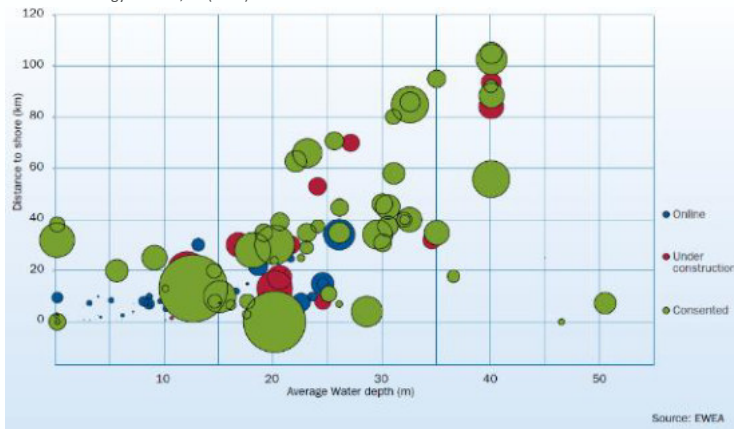




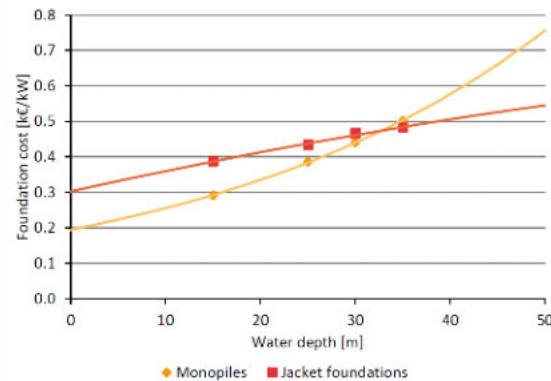
Substructures for online offshore wind farms till 2012

Source: Paraic Higgins and Aoife Foley, "The evolution of offshore wind power in the United Kingdom," Renewable and sustainable energy reviews, 37 (2014): 599-612.

Source: European Wind Energy Association(EWEA), Deep water. the next step for offshore wind energy, [http://www.ewea.org/fileadmin/files/library/publications/reports/Deep\\_Water.pdf](http://www.ewea.org/fileadmin/files/library/publications/reports/Deep_Water.pdf), 2013




Source: European Wind Energy Association(EWEA), Deep water. the next step for offshore wind energy, [http://www.ewea.org/fileadmin/files/library/publications/reports/Deep\\_Water.pdf](http://www.ewea.org/fileadmin/files/library/publications/reports/Deep_Water.pdf), 2013.



Monopile and jacket foundation costs for an 8 MW Wind Turbine

## AC Circuit Breaker – Highly reliable, cheap, matured technology




Energy Management

### DC commutation breaker successfully tested in 5000-A HVDC system in China

Erlangen, 2015-Jan-29

The Siemens MRTB DC commutation breaker (Metallic Return Transfer Breaker) with a rated current of 5000 ampere (A) has been successfully tested in its Xiluodu-Zhejiang high-voltage direct-current (HVDC) transmission system. Special breaker properties are required for transferring such high currents from one current path to another, a process also known as commutation. The circuit-breaker was integrated in the direct-current switchgear of the Shuaniong converter station and allows the uninterrupted switchover from grounding electrode mode to metallic return transfer mode and vice versa with no need for the operator to reduce the transmission power of the system. Until now, this only functioned with rate 5000 A. Siemens has now successfully exceeded this limit w thereby improving the operation, stability and reliability of this HVDC system in China.



## DC Circuit Breaker – Future technology

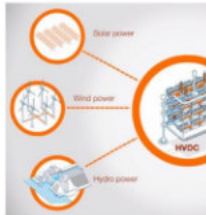


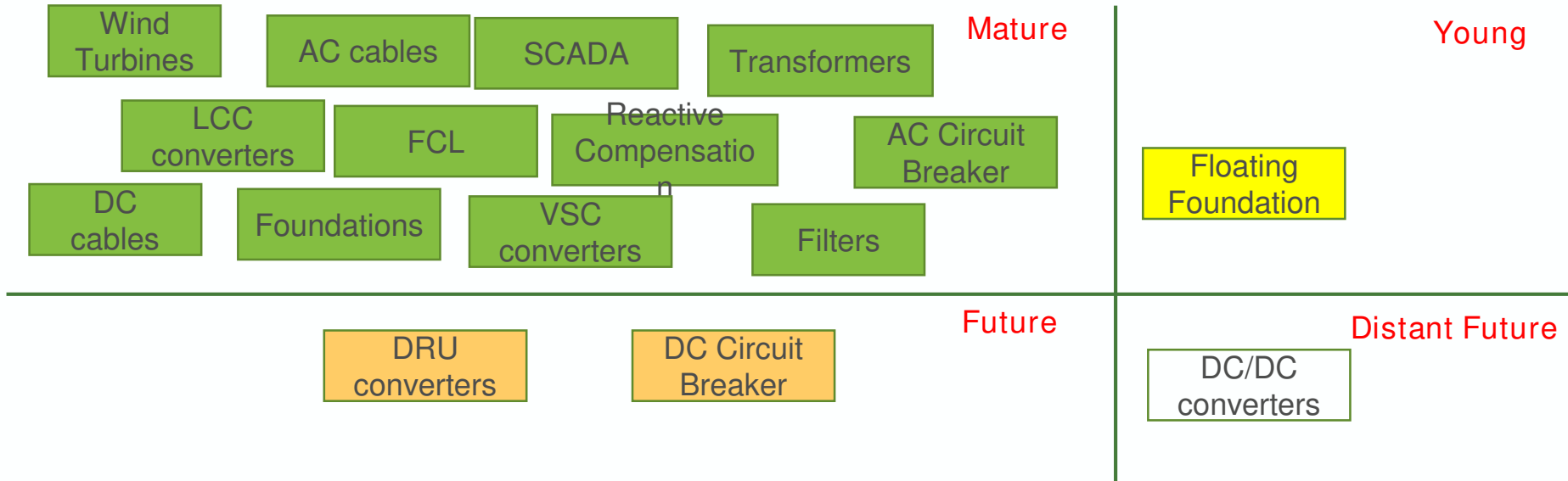
### ABB's Hybrid HVDC Circuit Breaker

#### Solving a 100 year old dilemma

Deployment of HVDC has led to an increasing number of [point to point connections](#) in different parts of the world. The logical next step is to [connect the lines](#) and optimize the reliability of the network. This will also enable balancing of loads, integration of intermittent renewables, lowering of transmission losses and facilitate energy trading across borders. Then why don't we just interconnect these lines into a grid? A major stumbling block or missing link has been the absence of an HVDC breaker that acts fast enough to interrupt current and isolate faults and at the same time keeps losses to a minimum.

[ABB's hybrid DC breaker](#) was developed after years of research, functional testing and simulation in the R&D laboratories. It is a breakthrough that solves a technical challenge that has been unresolved for over a hundred years and was perhaps one of the main influencers in the ['war of currents'](#) outcome. The 'hybrid' and power electronics switching that enables it to interrupt power flows unclear power station within 5 milliseconds – that's as fast as a honey bee takes than 30 times faster than the reaction time of an Olympic 100-meter medalist to react to the starter's gun! But it's not just about speed. The challenge was to do it 'ultra-fast' with minimal operational losses and this has been achieved by combining advanced ultrafast mechanical actuators with our inhouse semiconductor IGBT valve technologies or power electronics ([watch video: Hybrid HVDC Breaker – How does it work](#)).





- Mature: commercially available today; with (some) operational experience (TRL-9 today)
- Young: full scale prototypes available; very close to commercialization (TRL 6-8 today)
- Future: some prototypes available, but development still needed (TRL 4-5 today)
- Distant future: proof of concept and small scale prototypes, significant development still needed (TRL 1-3 today)



## Questions & Discussions

Thank You

