

# Master Thesis

at Carinthia University of Applied Sciences

10.11.2020



# Agenda

- Introduction and overview
- Master Thesis - **Michael Nowak** - Erarbeitung von Bewertungshintergründen zur Einschätzung der Brandwiderstandsdauer genieteteter Fachwerkträger aus Stahl (**Elaboration of assessment backgrounds to estimate the fire resistance of riveted steel trusses**)
- Master Thesis - **Johannes Molzbichler** - Umsetzung von Brandschäden in der Brandsimulation zur forensischen Analyse (**Implementation of fire damage in fire simulation for forensic analysis**)
- Master Thesis - **Sebastian Reiter** - Schwelbrandverhalten von Holz / Experimentelle Untersuchung der Abbrandgeschwindigkeit von Fichtenholz bei einem Schwelbrand (**Smoldering fire Behavior of wood / experimental investigation of the burning rate of spruce wood in a smoldering fire**)
- Master Thesis - **Lukas Treffner** - Ermittlung des Bauteilverhaltens und der Sanierbarkeit von Betondecken nach einem Brand (**Determination of the component behavior and the refurbishment of composite concrete slabs after a fire**)

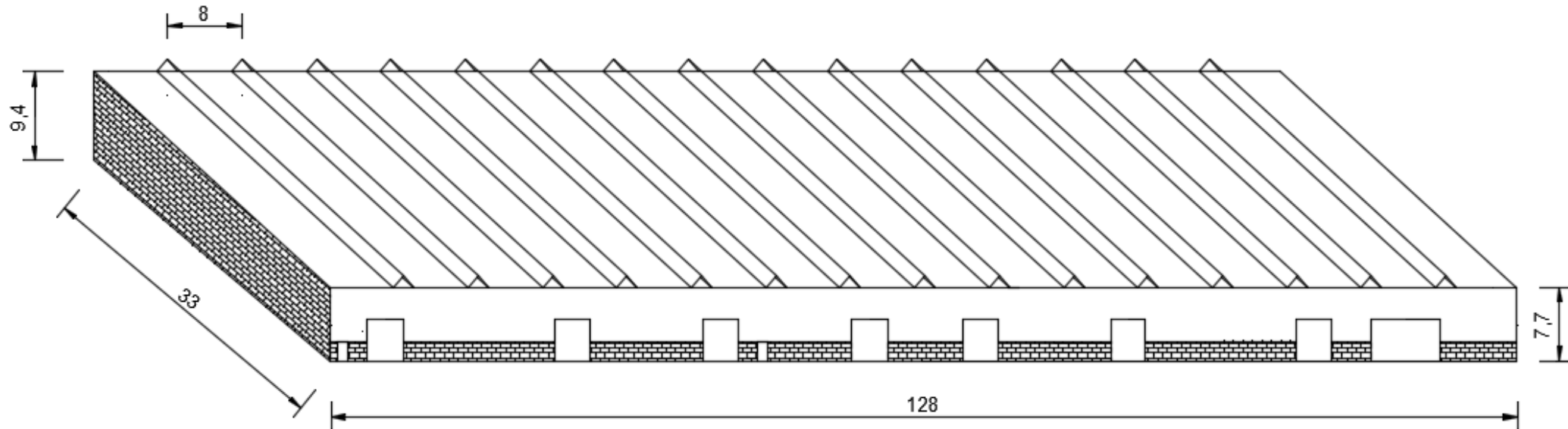
# Targets

- The example should show that by using fire simulation programs a determination of a realistic temperature determination in the fire room is possible.
- That leads to the more economical evaluation with regard to the profile dimensioning or when verifying during design of fire protection.
- Existing buildings can be retrofitted without any costly upgrades.

# Example

- Technikmuseum Historama – area 2.200 m<sup>2</sup>
- Exponates :
  - Antique car
  - Railways and trams
  - Fire engines and utility vehicles
  - Motorbikes
  - Carriages
  - Radio and telecommunication systems

# Example - Dimensions



# FRAMEWORK





# Example – stiffening between the bars



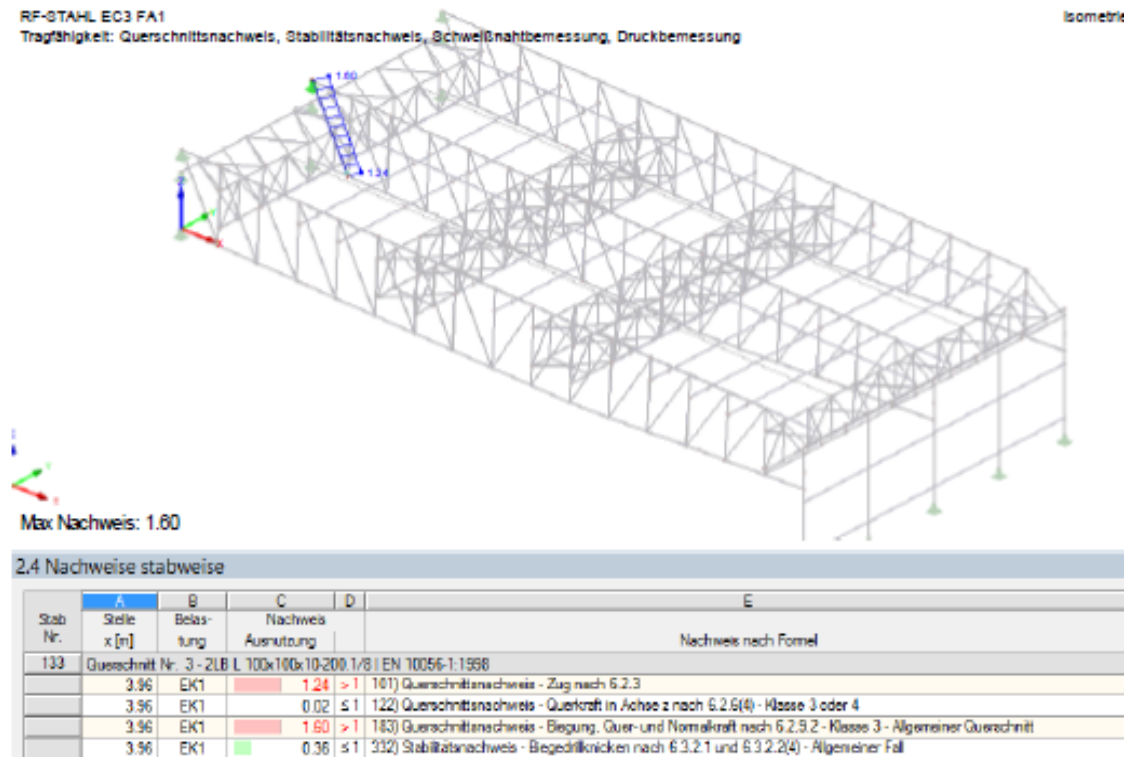
# Example – steel bar connected by rivets



- Stützen U 200
- Obergurt: L 100x150x15
- Untergurt L 100x100x13  
L 100x150x15
- Pfosten L 100x100x10  
L 90x90x9  
L 70x70x8  
U 160  
U 120
- Diagonale L 100x100x10  
L 80x80x12  
L 80x80x10



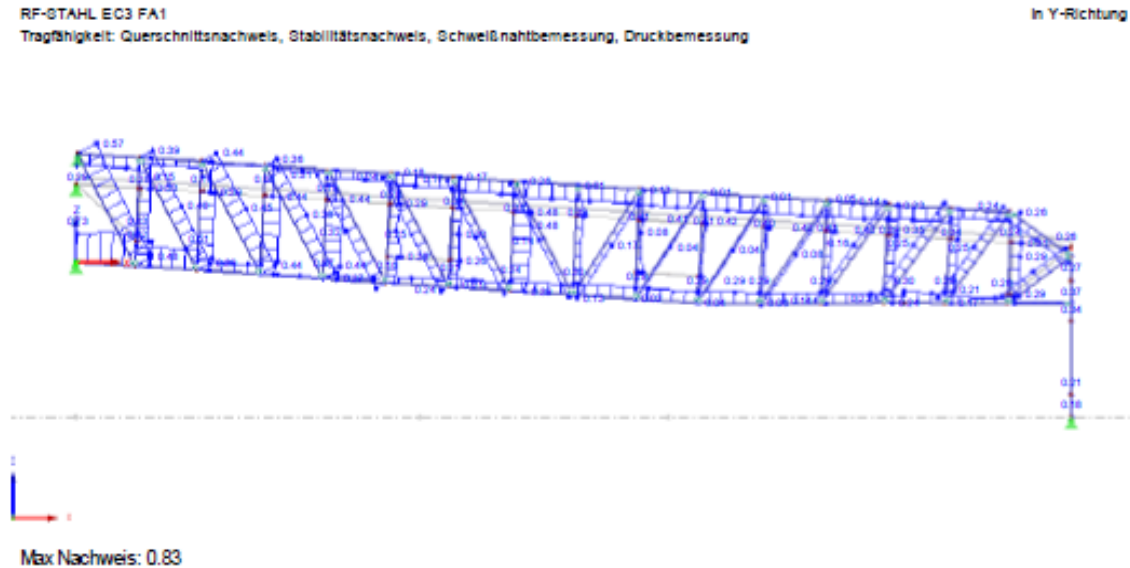
# Example – lead bearing capacity



# Example – race to the results (load factor)

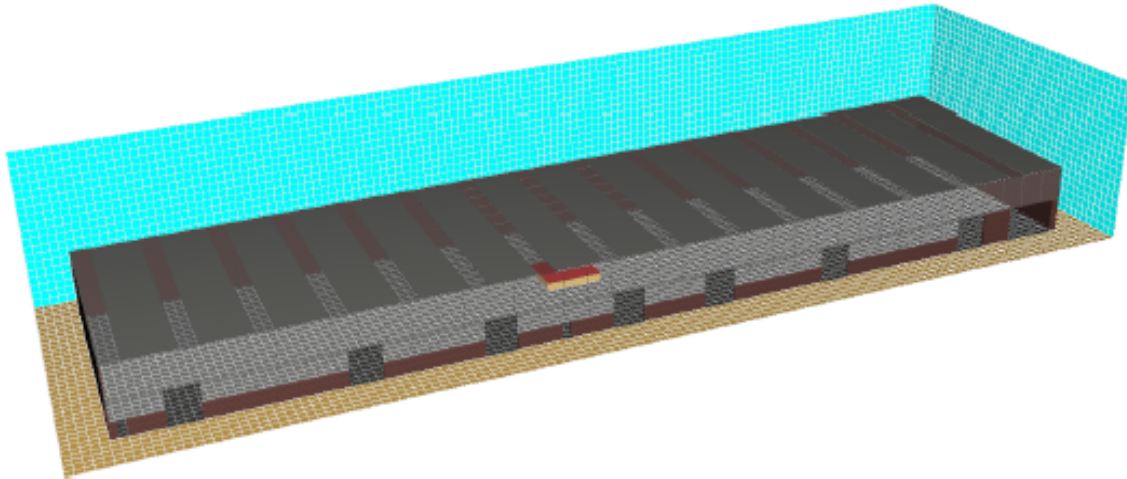
Profil	Ausnutzung nach Einheitstemperaturkurve [%]	Ausnutzung nach Simulationsergebnissen [%]	Ausnutzung bei Kaltbemessung [%]
2LA L 100x100x12- 220/6	134	87	51
2LB L 80x80x10- 200/8	133	86	45
2LB L 70x70x7- 205/8	631	107	48
2 UV U 200- 148/10	422	63	34

# Example – model for hot design



# Example – CFD model

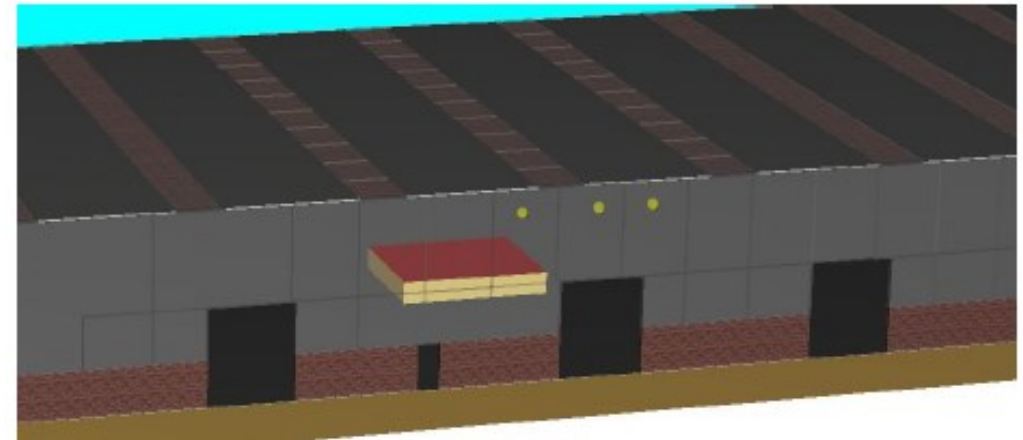
- Länge L = 140 m
- Breite B = 40 m
- Höhe H = 20 m.



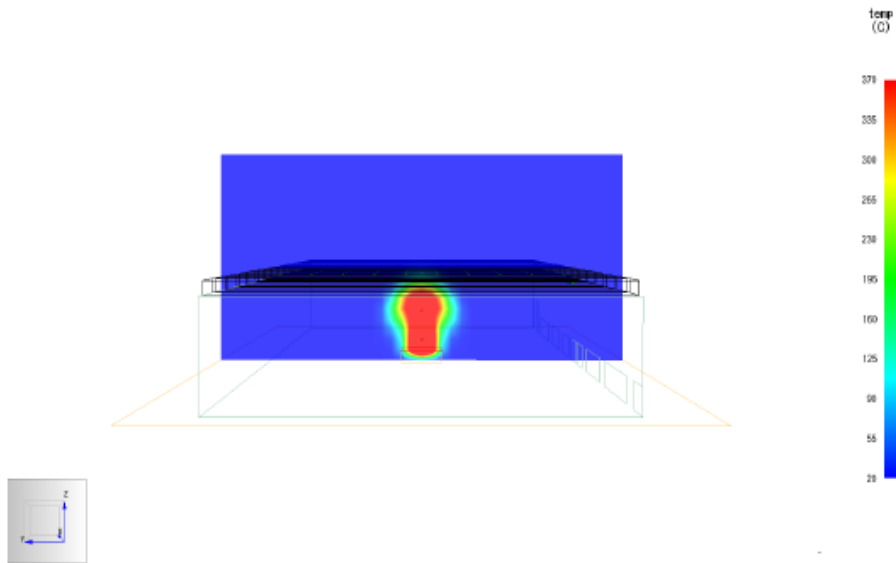
standard – glas in the roof breaks



alternativ – glas in the wall breaks



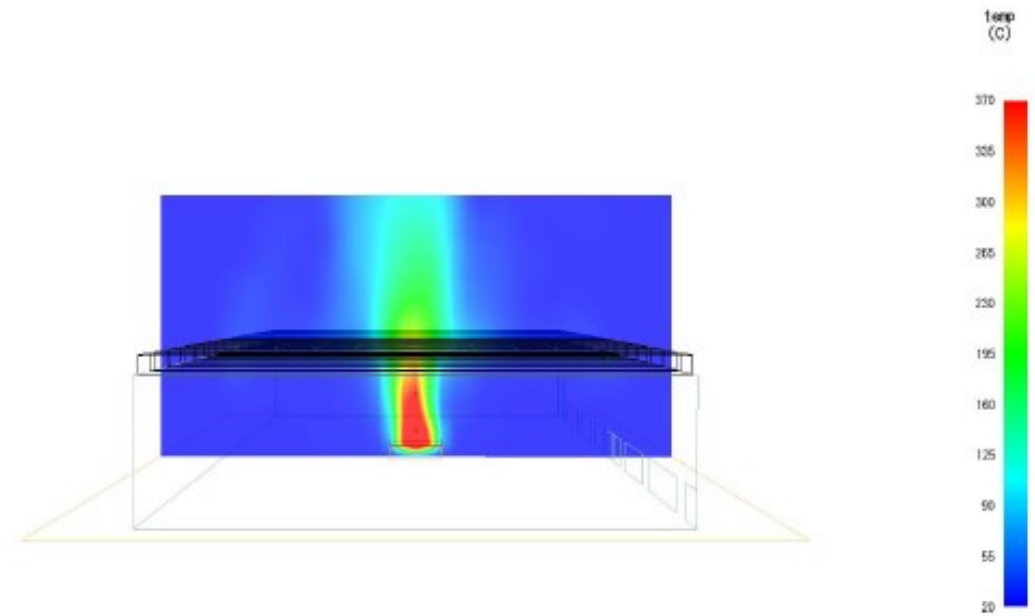
# Example – CFD model



What is the highest temperature at the surface of the bars?

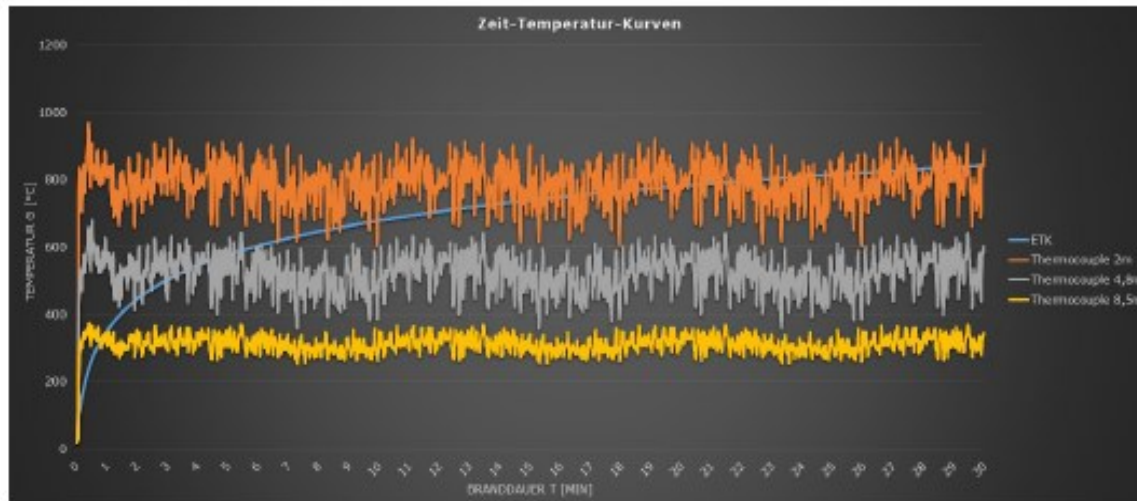


When does the glass break?





# Example – results / discussion

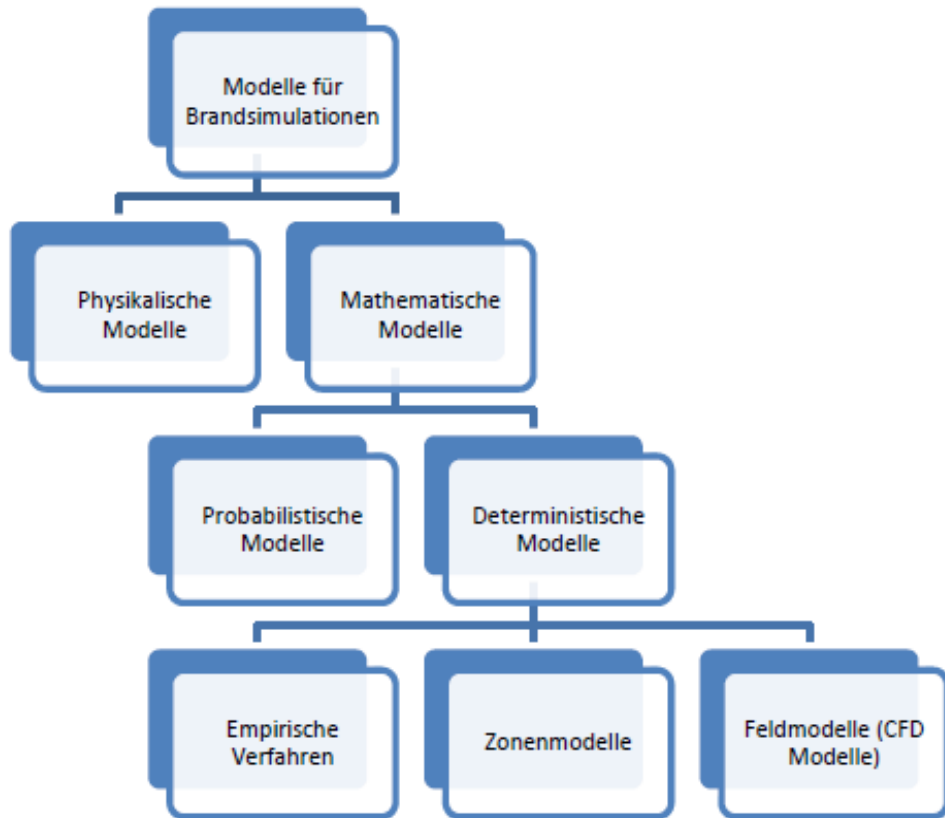


Ermittlung der Stahltemperatur auf Basis der Einheitstemperaturkurve				
Profil- und Materialangaben				
Stabtyp	Untergurt			
Profil	L	100x100x12		
Profilbreite	b	100	[mm]	0,10 [m]
Profilhöhe	h	100	[mm]	0,10 [m]
Profildicke	t	12	[mm]	0,012 [m]
Querschnittsfläche	A	22,70	[cm²]	0,00227 [m²]
Mantelfläche	$A_M$	0,39	[m²/m]	
Umfang	U	0,39	[m²/m]	
Profilfaktor	$A_M/V$	166,67	[1/m]	
Profilfaktor	$(A_M/V)_0$	176,21	[1/m]	
Rohdichte Stahl	$\rho_a$	7850	[kg/m³]	
Beiwerte				
Korrekturfaktor	$k_{sh}$	1,057		
Emissivität der Bauteiloberfläche	$\epsilon_m$	0,70		
Emissivität der Flamme	$\epsilon_f$	1,00		
konvektiver Wärmeübergangs-koeffizient	$\alpha_c$	25	[W/m²K]	
Konfigurationsfaktor	$\phi$	1,00		
Stephan-Boltzmann-Konstante	$\sigma$	0,0000000567	[W/m²K]	
Temperaturen nach 30 min auf Basis der Einheitstemperaturkurve				
ETK	$\theta_{ETK, 30min}$	842	[°C]	
Stahltemperatur nach ETK	$\theta_{s,ETK, 30min}$	824	[°C]	

# Targets

- The aim of the work is the reconstruction (determination of the cause of the fire) of the church fire.
- The simulation software PyroSim is used for this, which represents a graphical user interface for the Fire Dynamics Simulator (FDS).

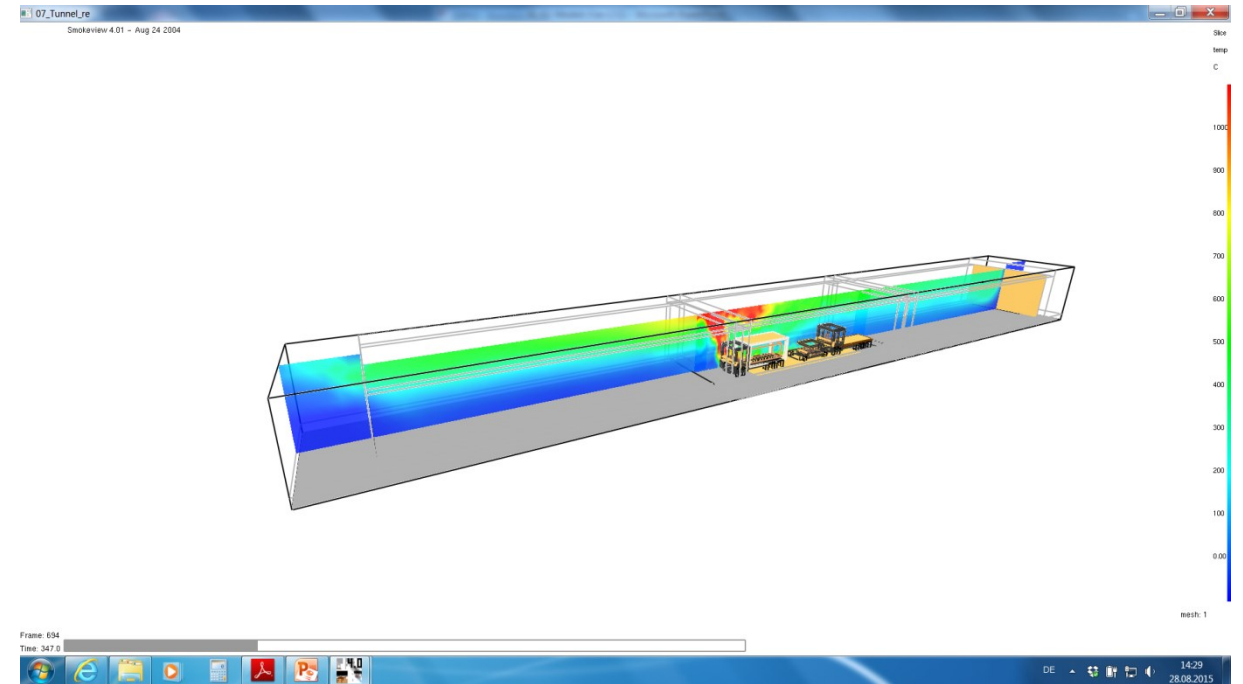
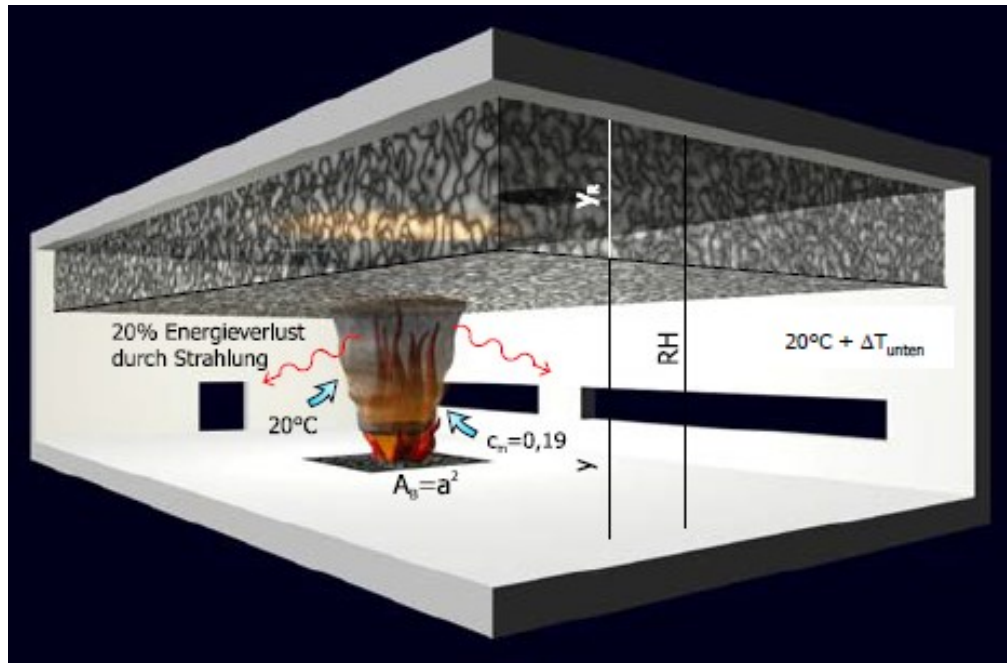
# Simulation models



Properties	Analytic methods	Simulation models
temporally development	no	yes
scaling	only for allowed range	yes
plausibility check	easy	easy to complex
error estimation	easy	difficult
complexity	low	middle to complex
information	individual information	system information

# Simulation models

MRFC



# Simulation models

Properties	Zone model	Field model
geometry	estimated	exact
ventilation	exact	exact
heat source	estimated	estimated
complexity	low	very high
information	global	local
verification	complex	very complex
plausibility check	easy	complex
depends on dimension	not possible	very high
accuracy	estimated	depends on cell size
costs	low	very high



# Forensic

- understand the course of the fire (how did the fire develop, what effect do different ventilation conditions have, etc.)
- Analysis of traces of fire (burn-off of fire loads, effect of temperature on surfaces, etc.)
- Visualization of the fire event (three-dimensional visualization of the fire event)
- Checking the timing of a fire event (rate of fire spread, smoke spread, activation and effect of fire protection devices, etc.)
- Checking the survival conditions of people (exposure to heat, flames and smoke gases, visibility, etc.)
- Review of different hypotheses about the course of the fire

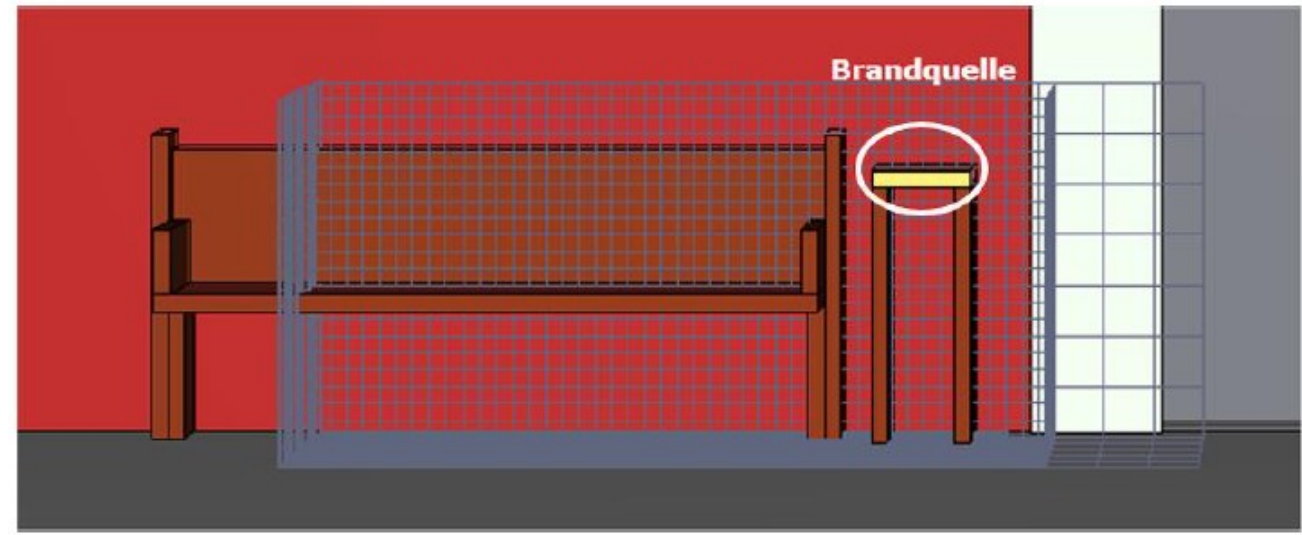
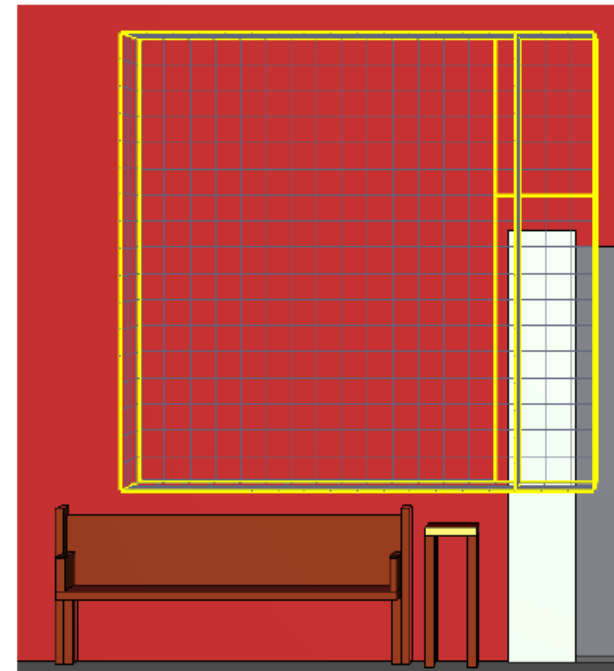
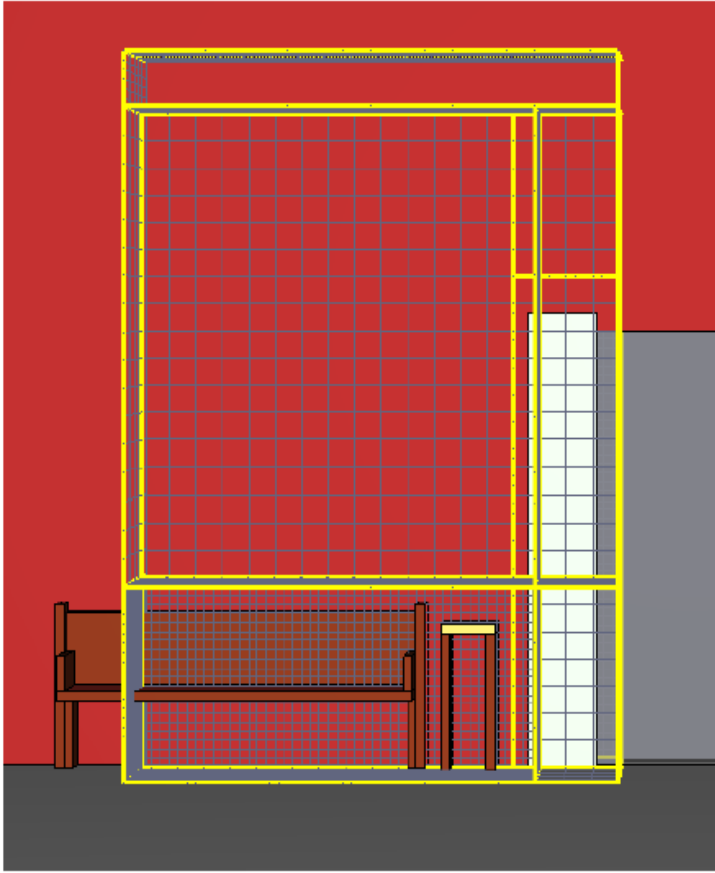
# Example



# Example



# Example - Simulation



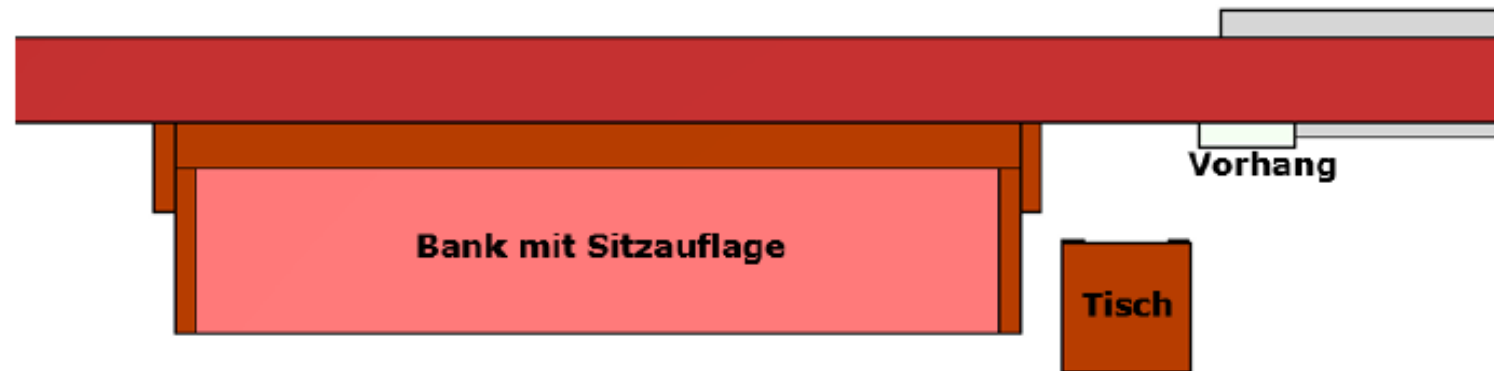


# Example – Simulation (fire load)

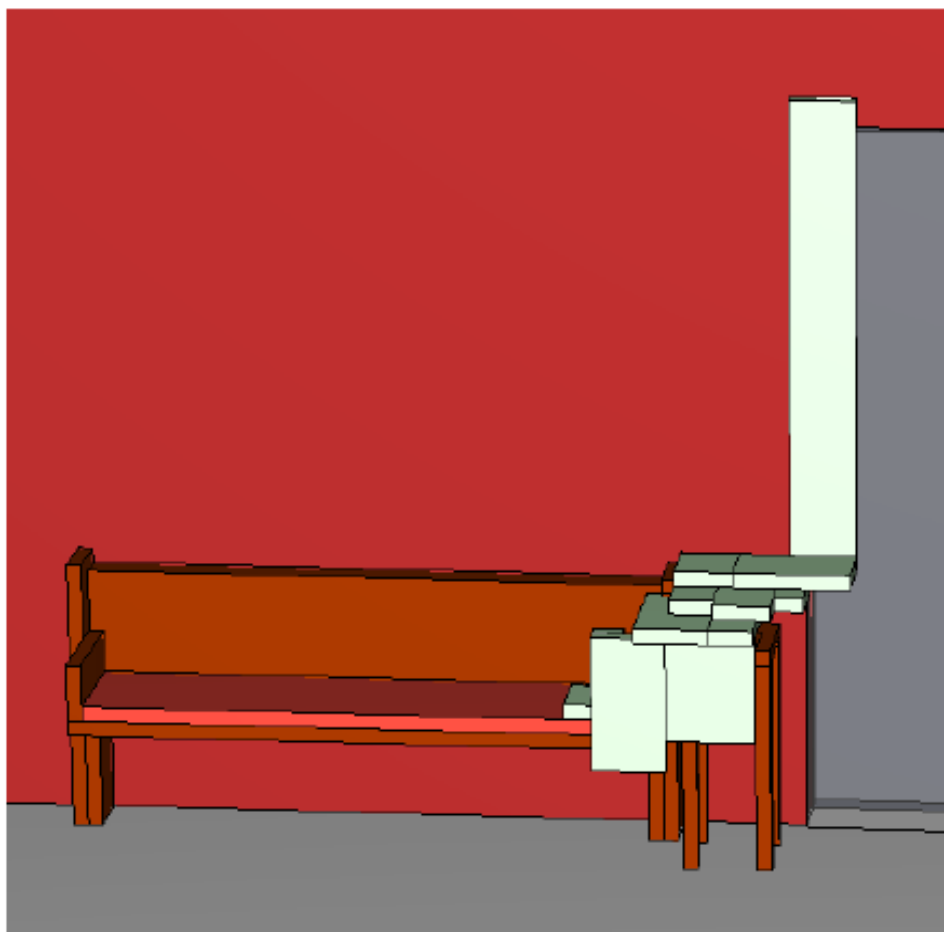
Brandlast	Thermophysikalische Eigenschaften	Farbe im Modell (siehe Abbildung 49)
Bank	Eichenholz*	braun
Orgelstuhl	Eichenholz*	braun
Sitzauflage Bank	Polsterstoff*	hellrot
Vorhang	Vorhangstoff*	hellgrün



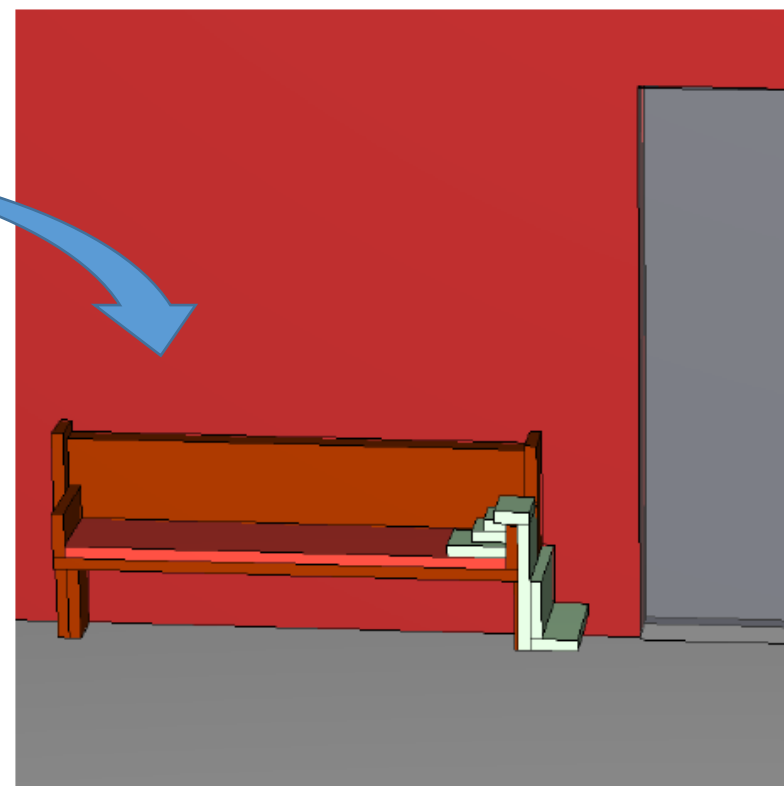
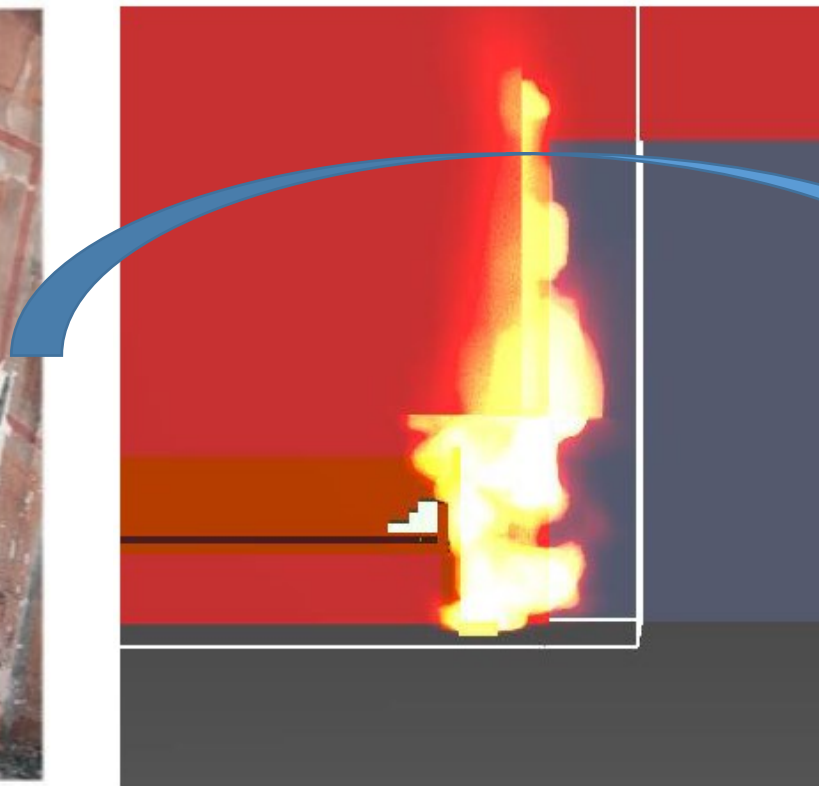
# Example – Simulation set



# Example – Simulation set

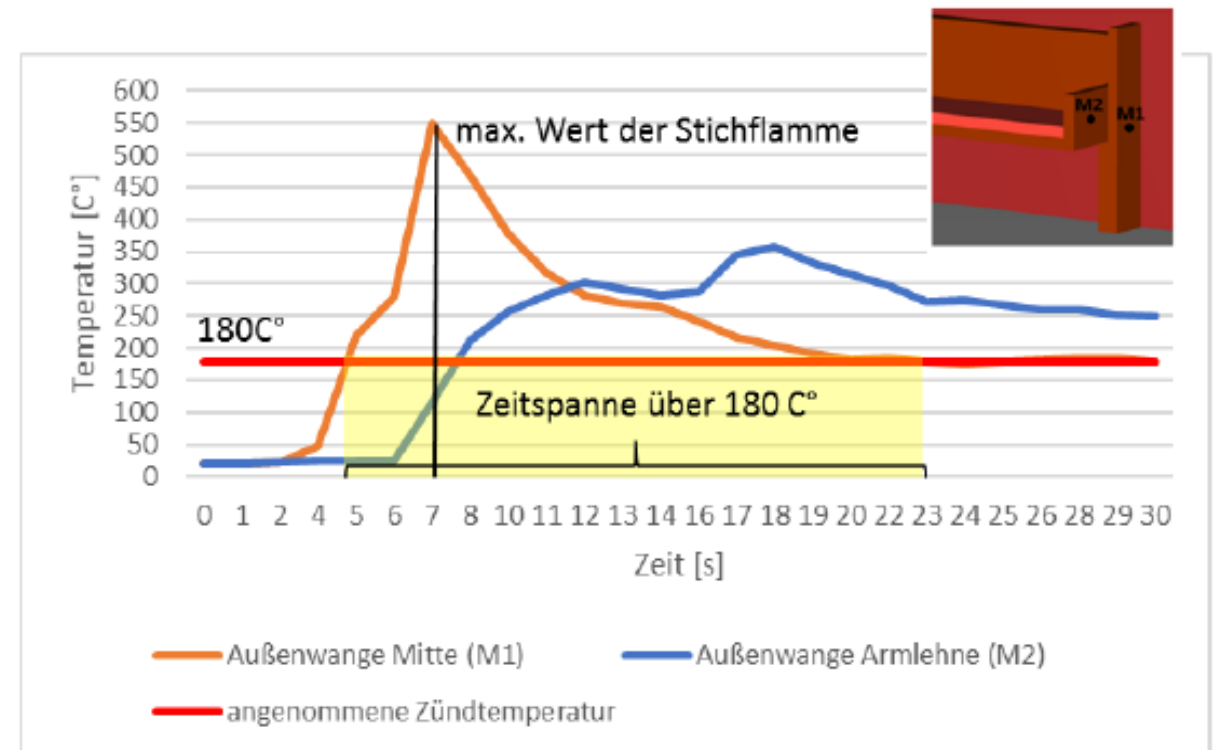
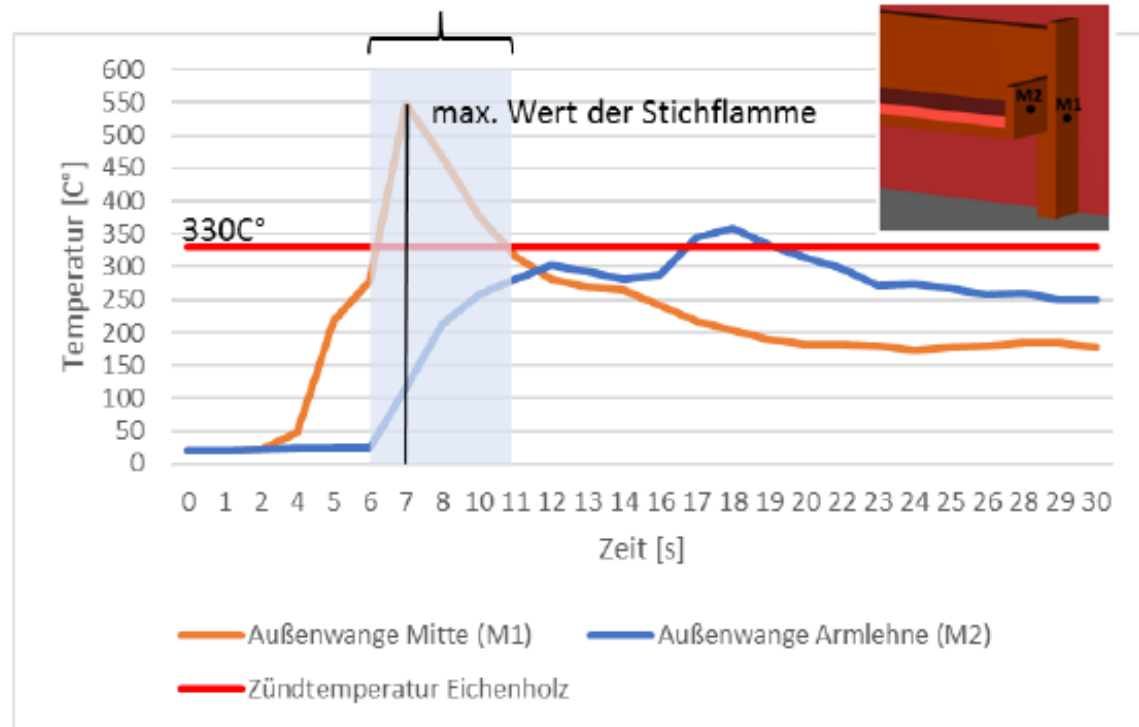


# Example – Simulation set



# Example – Simulation results

Zeitspanne ca 5 Sekunden mit Temperaturen über 330 C°

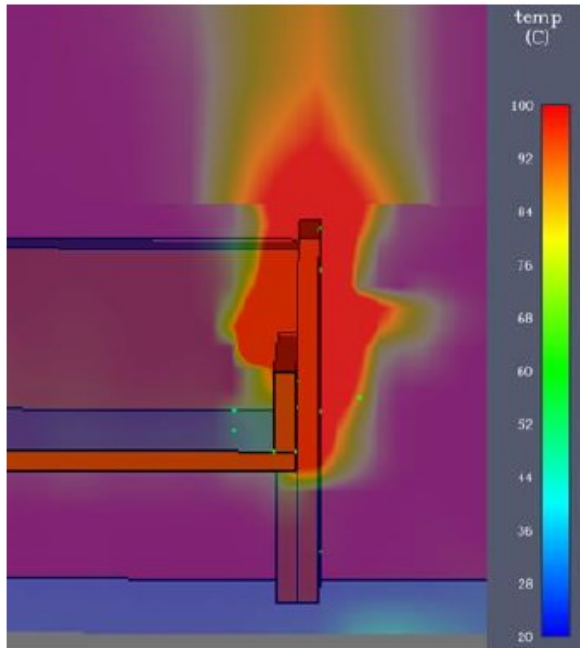


# Example – Simulation results

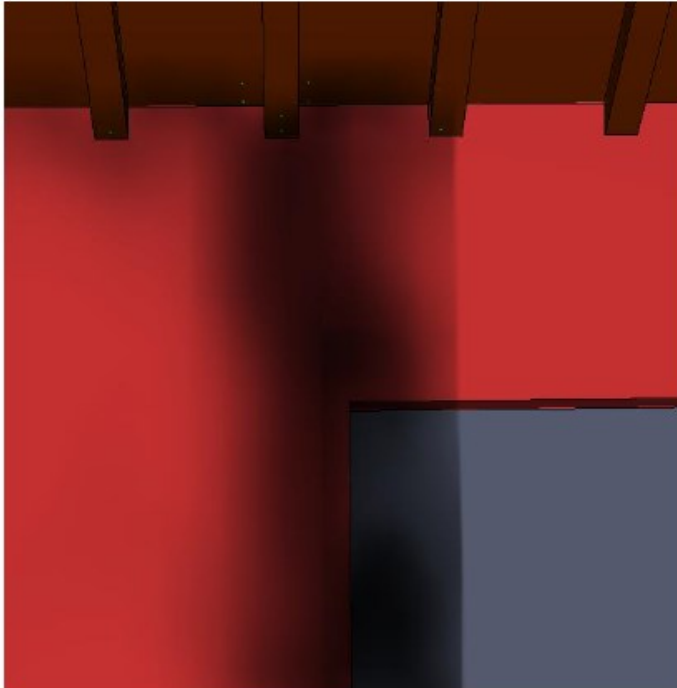




# Example – Simulation results



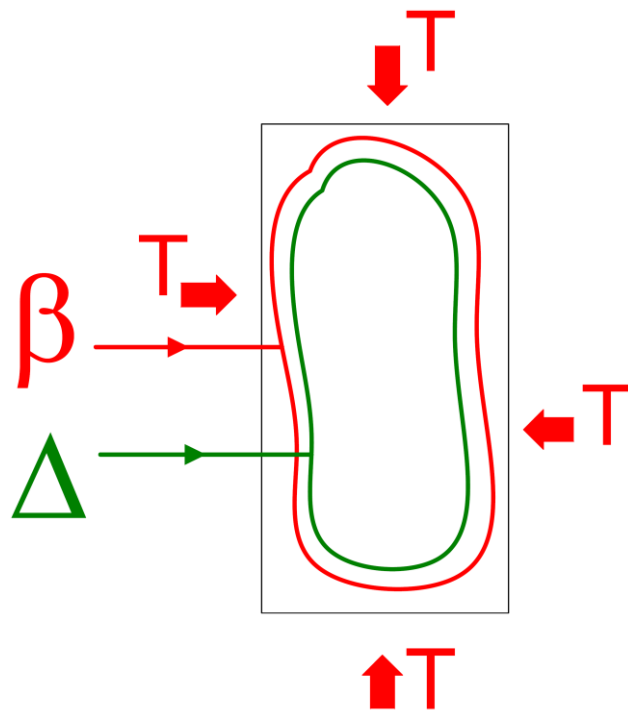
# Example – Simulation results



# Targets

- The development of a corresponding test facility to carry out smoldering fire tests.
- The test results should be used to determine whether and to what extent the rate of combustion of spruce wood in a smoldering fire changes compared to the rate of combustion related to the standard fire, and whether this confirms the influence of the temperature and the combustion air supply on the rate of combustion.

# Background



- continuous, slow fire
- combustion rate ca. 0,7 mm/min
- no dropping, no melting
- small heat conductivity
- insulation of wood charcoal layer
- load bearing capacity is given for a long time
- no collaps
- Good estimation of end of the load bearing capacity

Eq. combustion layer:

$$d_{char} = \beta \cdot t$$

# Background – Smoldering fire

## Smoldering fire

Drying



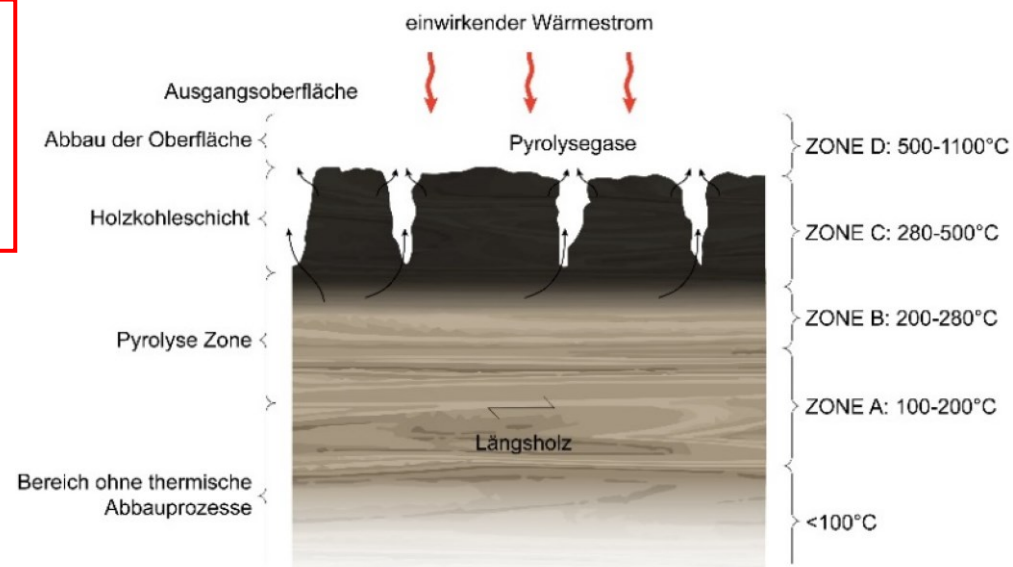
Pyrolysis



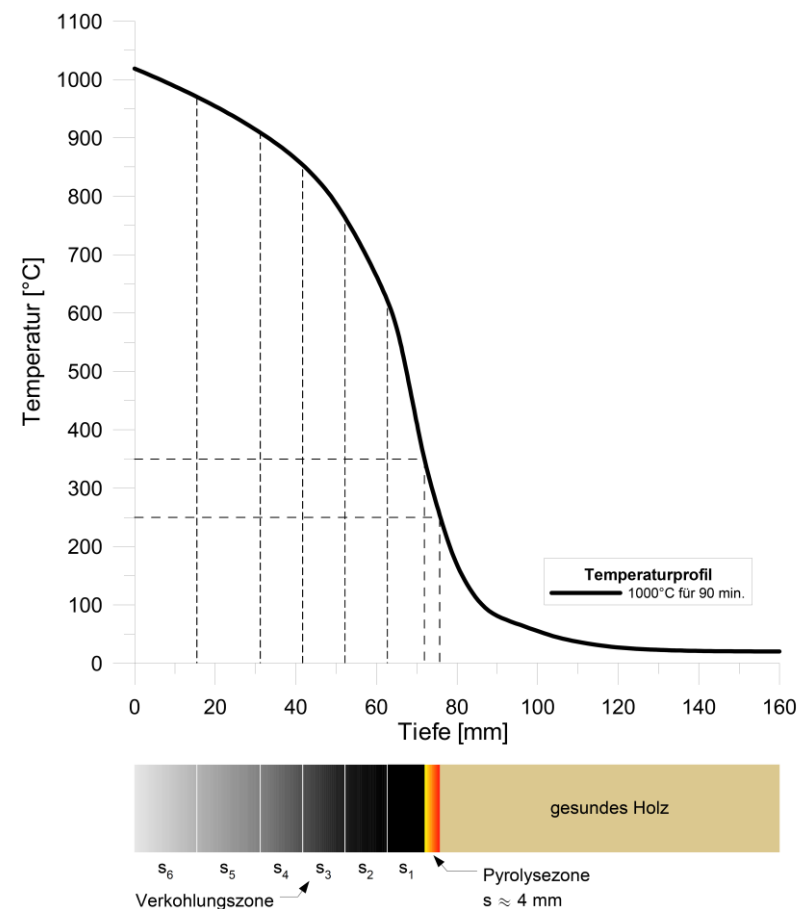
Combustion of  
fire gases



Combustion of  
the wood  
charcoal



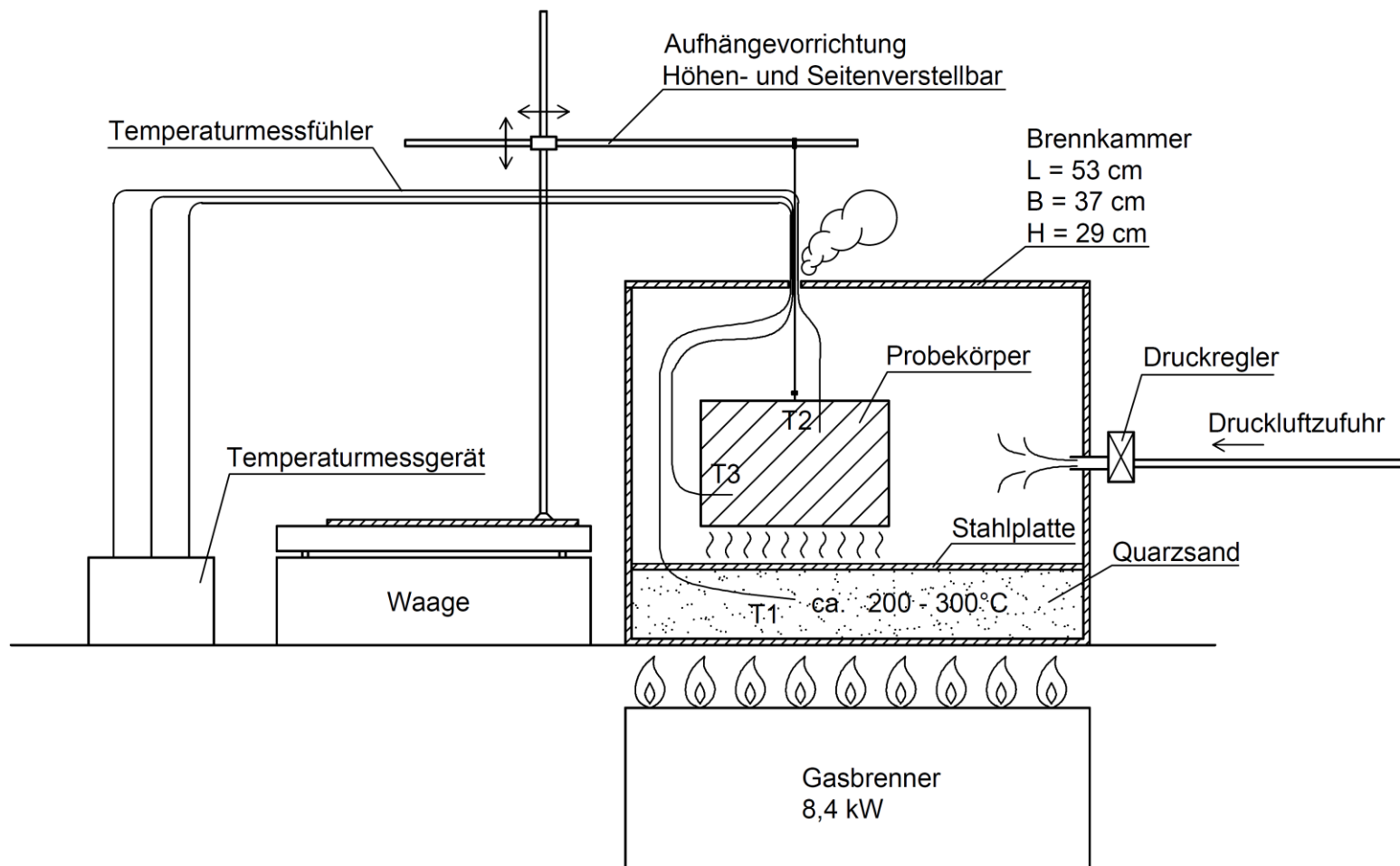
Zones of wood fire



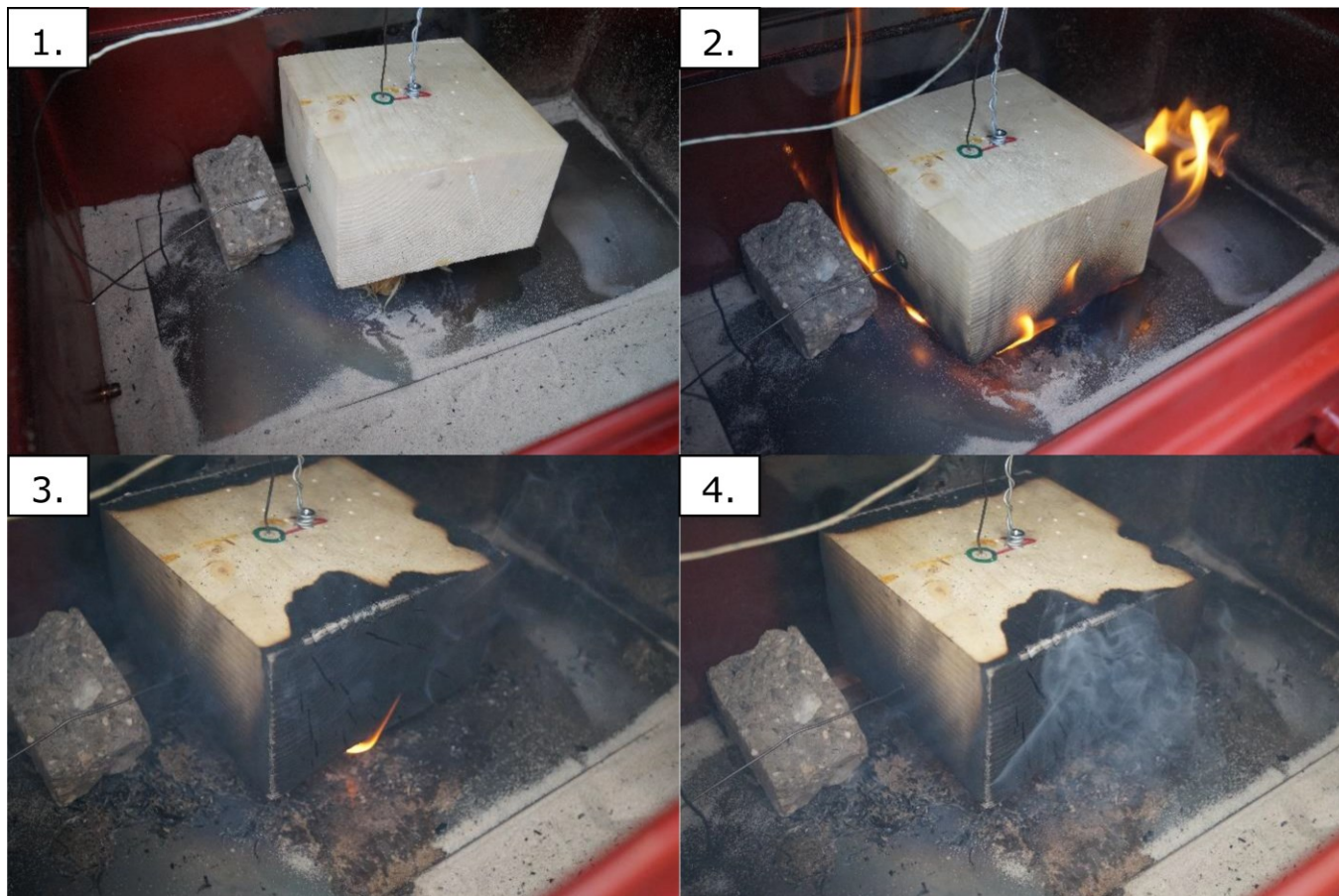
Temperature distribution in the wood cross section



# Test setup





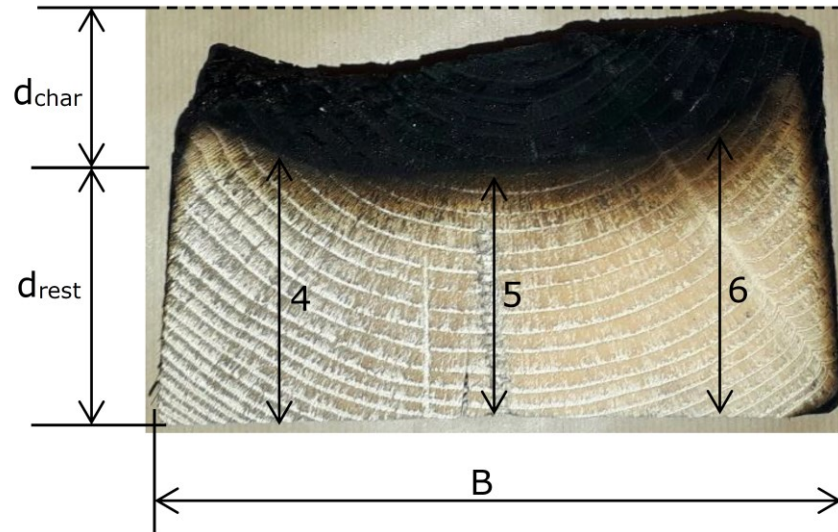
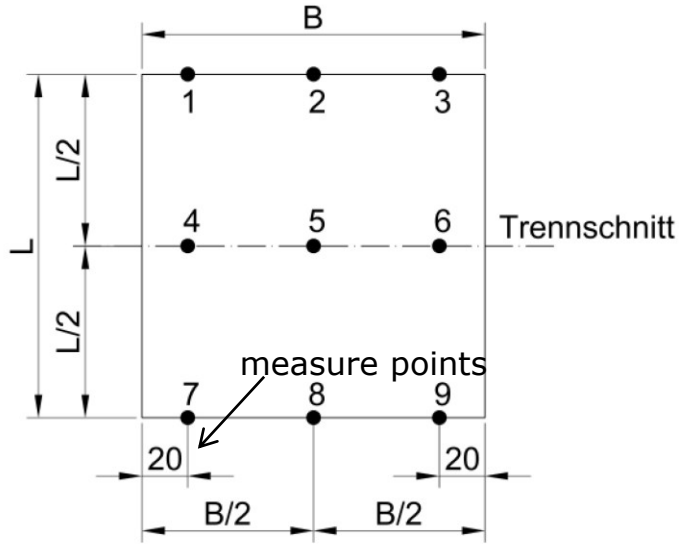


1. Specimen in the combustion chamber

2. Start of combustion

3. Subside of flame

4. Start of smoldering fire



1. Quenching of specimen
2. Cut the specimen for measuring
3. Clean the surface
4. Check the residual high
5. Calculate of  $\beta$

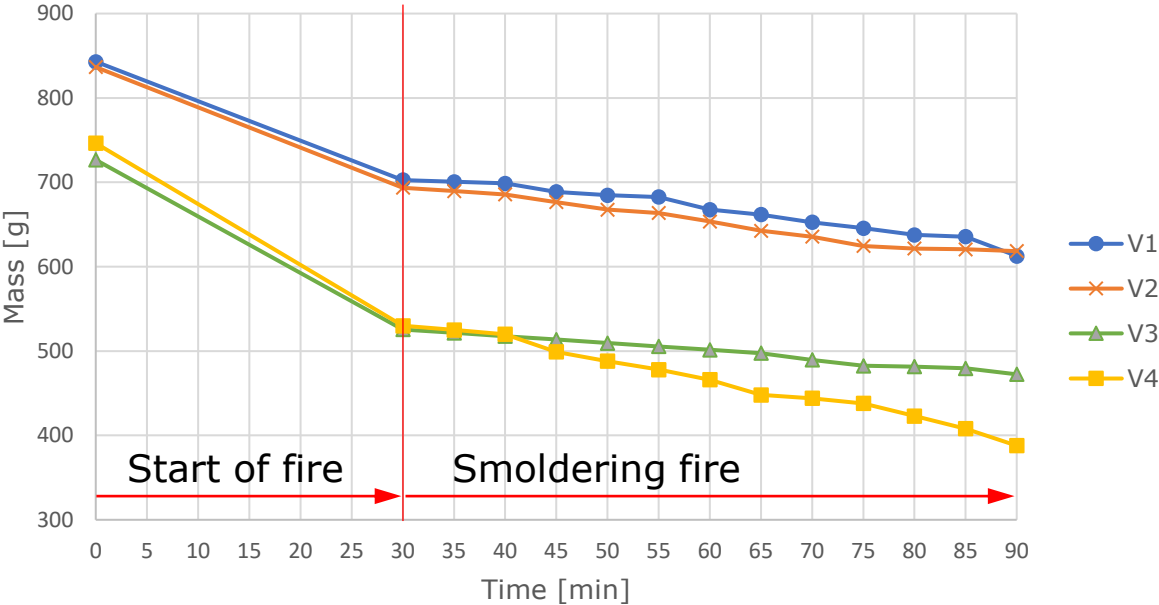
$$d_{char} = d_0 - d_{rest}$$

$d_0$  origin high

$d_{rest}$  residual high

$d_{char}$  combustion rate

$$\beta = \frac{d_{char}}{\Delta t}$$

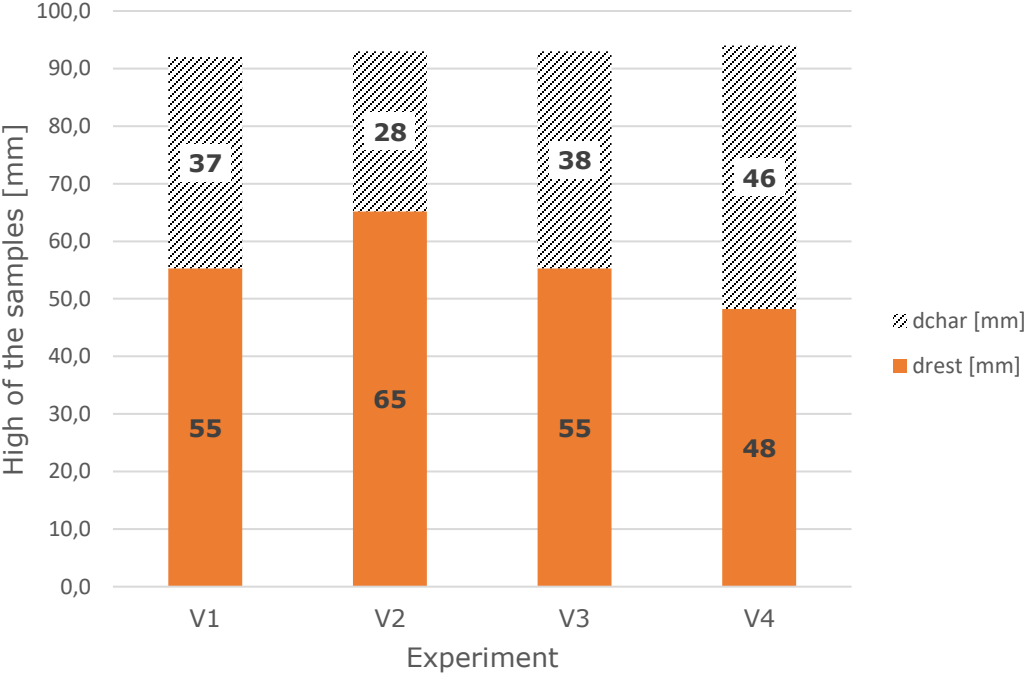
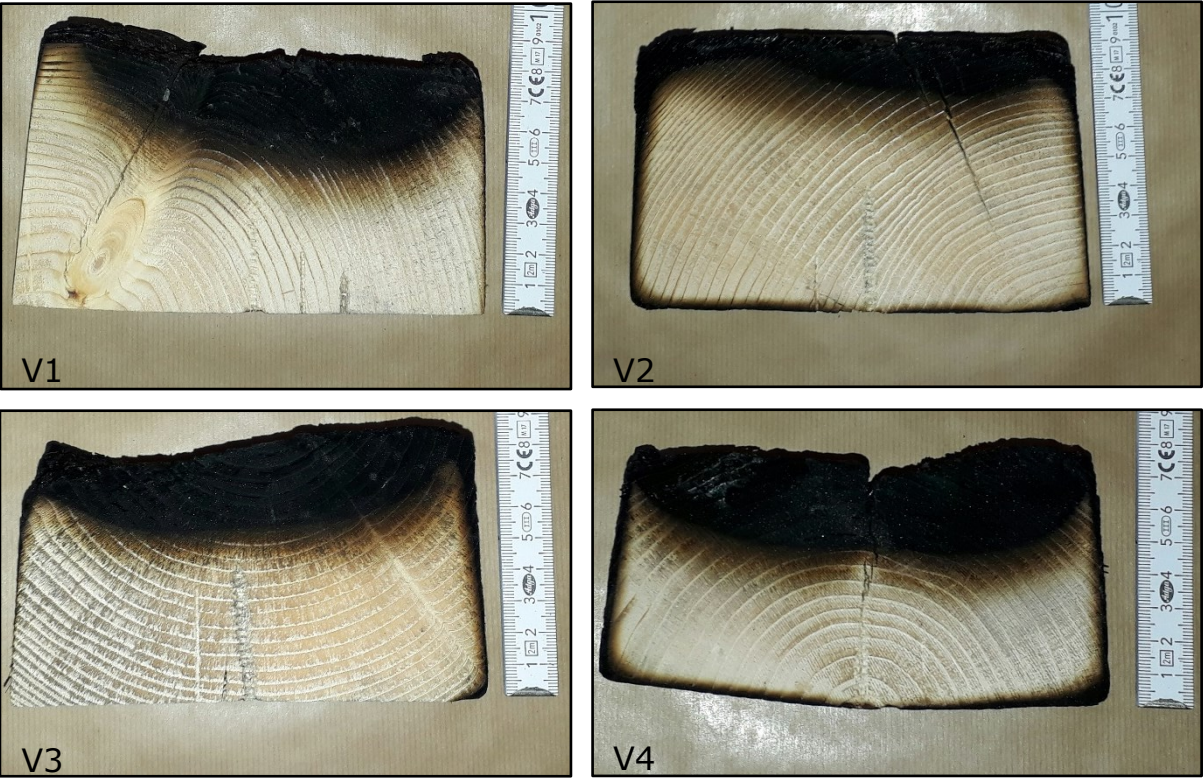


Exper.	m <sub>1</sub> [g]	m <sub>2</sub> [g]	Δm [g]	Δt [min]	ṁ [g/min]
V1	842,8	612,6	230,2	90	2,6
V2	836,6	618,5	218,1	90	2,4
V3	726,5	472,5	254,0	90	2,8
V4	746,2	387,9	358,3	90	4,0

loss of mass

$$\dot{m} = \frac{(m_1 - m_2)}{\Delta t} \approx 3 \text{ g/min}$$





# Comparison

Exp.	$\Delta t$ [min]	$d_0$ [mm]	$d_{rest}$ [mm]	$d_{char}$ [mm]	$\beta$ [mm/min]
V1	90	92,0	55,3	36,7	0,41
V2	90	93,0	65,2	27,8	0,31
V3	90	93,0	55,3	37,7	0,42
V4	90	94,0	48,2	45,8	0,51
Average				37,0	0,41

$$\beta = \frac{d_{char}}{\Delta t}$$

average combustion rate  $\beta$  =  
0,41 mm/min

Experiment	max. Temp.	Duration	Comb. Layer	Comb. Rate
Werther [6]	ca. 600 °C	60 [min]	27 [mm]	0,44 [mm/min]
Fornather [37]	ca. 700 °C	90 [min]	38 [mm]	0,42 [mm/min]
Reiter	ca. 400 °C	90 [min]	37 [mm]	0,41 [mm/min]

fully dev. fire  
 $\beta$  = 0,65 mm/min

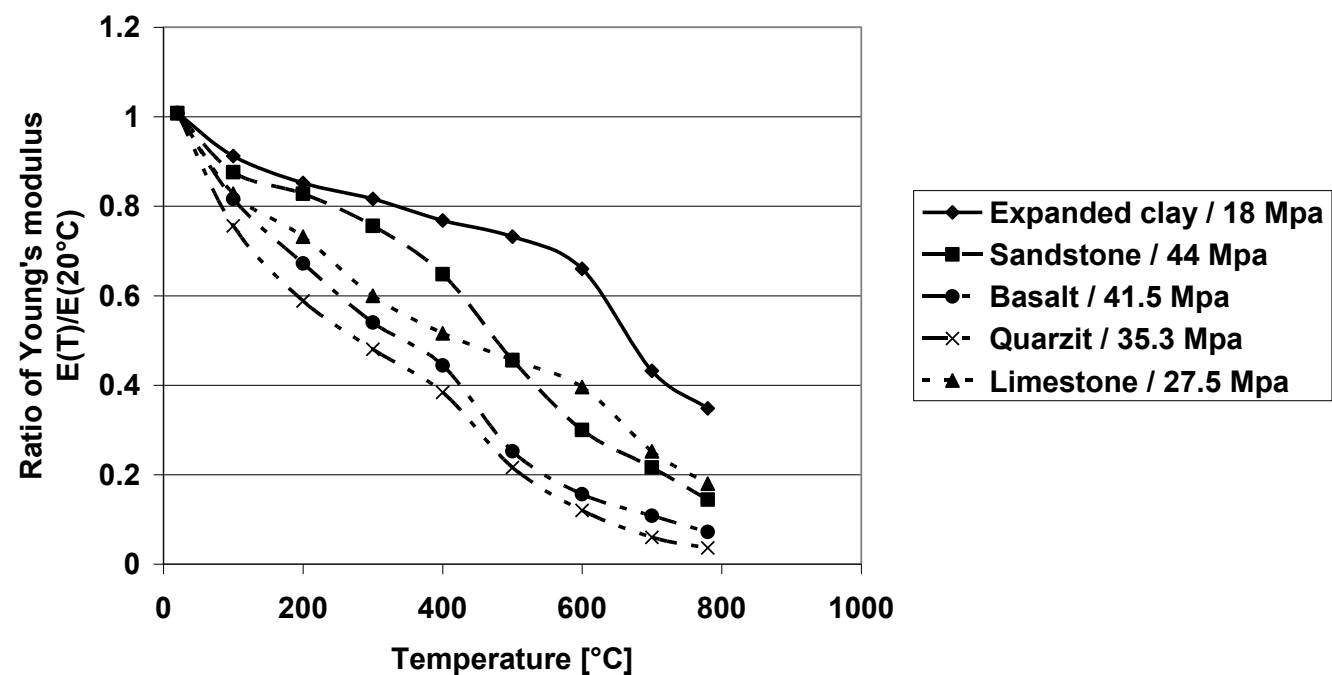
Smoldering fire  
 $\beta$  = 0,4 mm/min

# Targets

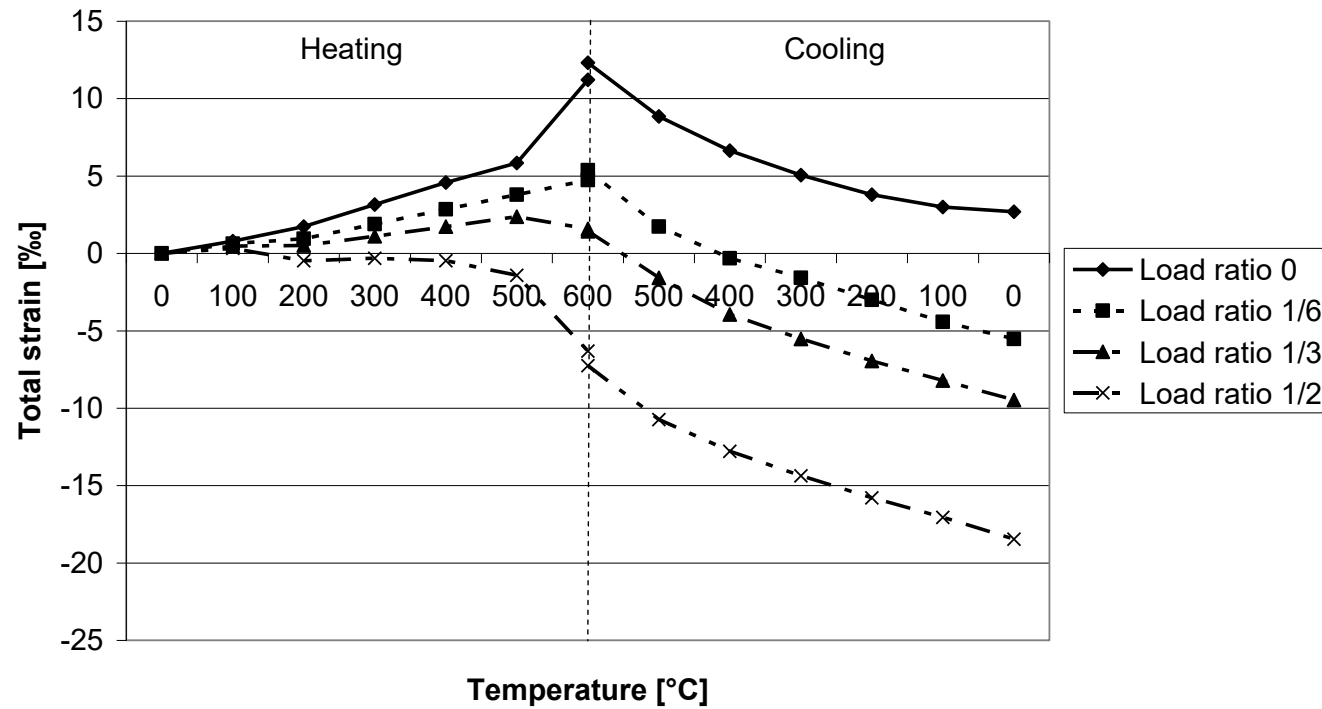
- Parameter study for determination of residual behavior after fire damage
- Behavior of composite slab during and after fire
- Refurbishment of fire damage



# Parameter study



# Parameter study



# Experiment

- Variation of:
  - concrete C25/30, C35/45
  - mortar sealing
  - gypsum board
  - plastic pipes between reinforcement and cover
  - Cooling
  - Joint and bond in composite slab

# Experiment – composite slaps



# Experiment – store (90 d) and preparation



# Experiment – fire test





# Experiment – fire test



# Results



Mortar, small spallings



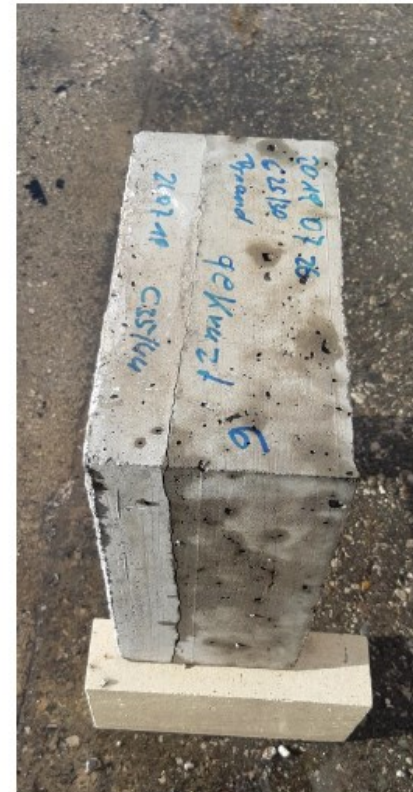
Gypsum,  
no sealing with paper  
gypsum is damaged



C25/30,  
only carbon black



# Results – composite slaps



# Results – Parameter – Compressive strength

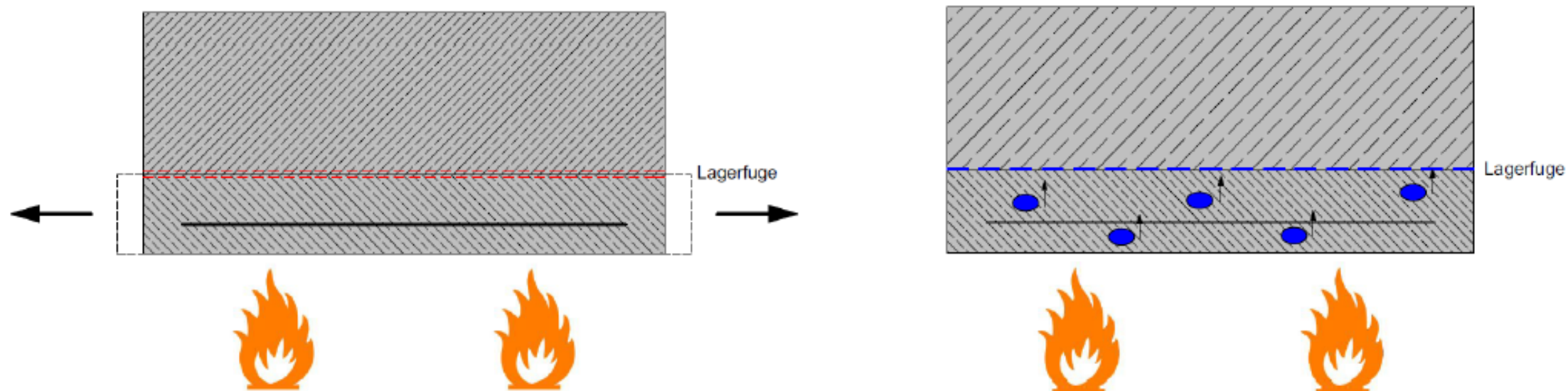
Surface sealing during fire	Decrease in %
Gypsum	20.5
Concrete	35.25
Mortar	32.0

# Results – Parameter – tensile adhesive strength



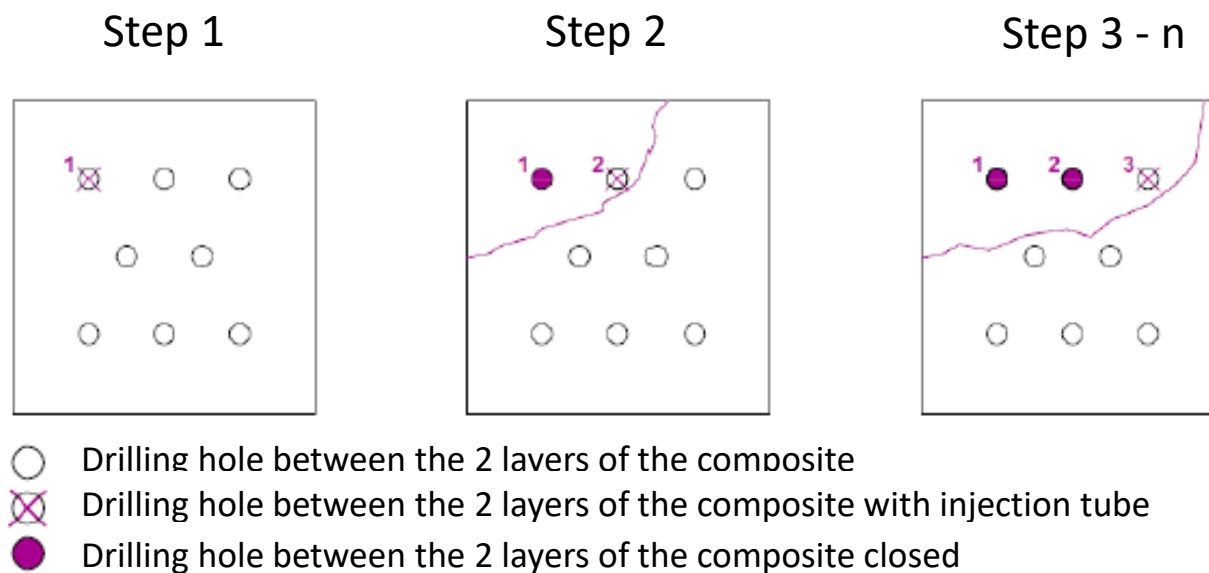
Experiment	Concrete + surface	tensile adhesive strength (MPa)
1	C35/45 plain concrete	1,8
2		1,7
3	C35/45 mortar	2,2
4		1,5
5	C35/45 gypsum	2,0
6		1,7

# Discussion composite slaps





# Discussion composite slaps



# Thank you.

- Questions?
- Comments?